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(54) Title: POWDER COATING COMPOSITIONS (57) Abstract <p>The invention provides a powder coating composition in which powder particles are an agglomerate of individual particulate components fused or bonded together into composite particles, wherein the individual particulate components comprise coloured film-forming base components having a Dv.99 of no more than 30µm, and one or more uncoloured film-forming components, at least one component (2a) having a Dv.99 that is more than 20µm and that is higher than the Dv.99 of the coloured components taken together, the ratio of coloured film-forming base component(s) to uncoloured film-forming component(s) in the composition being in the range of from 1:99 to 60:40 by weight. Maximising the amount of larger-sized uncoloured component(s) gives cost advantages, and the invention allows a rapid and flexible manufacture of a range of coloured powder coating compositions.</p>		

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POWDER COATING COMPOSITIONS

FIELD OF THE INVENTION

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This invention relates to powder coating compositions and to their use.

Powder coating compositions generally comprise a solid film-forming resin, usually with one or more colouring agents such as pigments, and optionally they also contain one or more performance additives. They are usually thermosetting,
10 incorporating, for example, a film-forming polymer and a corresponding curing agent (which may itself be another film-forming polymer).

The compositions are generally prepared by intimately mixing the ingredients (including any colouring agents and performance additives) for example in an extruder, at a temperature above the softening point of the film-forming polymer(s) but below a
15 temperature at which significant pre-reaction would occur. The extrudate is usually rolled into a flat sheet and comminuted, for example by grinding to the desired particle sizes ("micronising"). The size distribution required for most commercial electrostatic spray apparatus is up to 120 microns, often between 10 and 120 microns, with a Dv.50 within the range of 15 to 75 microns, preferably 25 to 50 microns, or more especially 20
20 to 45 microns.

BACKGROUND TO THE INVENTION

Currently, powder coating manufacturing methods allow the manufacturer to
25 offer commercially a range of full gloss coatings in a variety of colours. The range of products available in reduced-gloss finishes is, however, limited.

Reduction of gloss to some other lower level, for example satin gloss (55-65% gloss) or matt (< 30% gloss), is achieved by creating a surface which is rough on a microscopic scale. This may be achieved by using incompatible components or components that generate incompatibility. For example, an acrylic component and a polyester, epoxy, polyester-epoxy or polyurethane component are incompatible, and cannot be blended to form a single (stable) phase. Incompatibility during film formation can also be achieved by using components that are initially miscible (compatible) but that become incompatible during curing. Thus, for example, two systems of similar chemistry and approximately the same gel time are compatible, but components with different gel times are initially compatible but become incompatible as curing (and molecular weight build-up) proceeds. Thus, gloss-reducing agents include a second catalyst which will give a much faster gel time than the principal catalyst used to cure the film. Alternatively, with acid-functional polyesters, for example, a fast gelling (reacting) powder and a slow gelling powder may be manufactured separately using polyesters of different functionality, and mixed after the micronising stage or, more usually, the components are mixed prior to micronising; the components should have the same colour and particle size. Production of small batches of reduced-gloss coating composition, however, is uneconomic. A different method utilises a product called 'gloss killer', available from the company Tiger, which is mixed in after the micronising stage. However, this product, a clear (uncoloured) powder coating, can be added only in limited amounts to a conventional coloured powder coating before the presence of the gloss killer can be detected from the sparkle generated by the particles of the clear gloss killer powder in the film. Therefore the product is limited to adjusting gloss by a few percentage points.

There is accordingly a need for powder coating compositions in a wide range of reduced-gloss finishes, which avoid the problems mentioned above.

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Speed of delivery to customers is also an important consideration, but the conventional powder coatings manufacturing method relies on premixing, extrusion and milling as separate processes, causing turnaround times to be long, and production of small batches of a product is again not economic. Stocking large product ranges solves the problem of speed of delivery, but is a highly inflexible approach and is not cost-effective.

EP 372860 A describes a colour mixing process for powder coatings in which sufficiently small-sized particles ($< 20 \mu\text{m}$ in size and advantageously $< 10 \mu\text{m}$) are used that mixed colours applied to a substrate have a homogeneous appearance.

10 Before application to the substrate the mixture is generally subjected to a process of agglomeration in which the small-sized particles are fused or bonded into composite particles, for example by mechanofusion, to convert the mixture from a cohesive mass to a free-flowing and fluidisable powder, which can be applied by conventional means. Thus, a range of basic coloured powder coating compositions is produced,

15 conventionally, in a conventional melt extrusion step, and the products are comminuted to a distinctively small particle size. A range of other colours can then be produced by mixing and agglomerating these coloured powder bases in the desired proportions. This allows the storage of comparatively few basic coloured powder bases, which can be mixed and agglomerated to produce any desired shade easily on demand, and the

20 production of small quantities becomes commercially feasible.

An extension of this agglomeration technique for the flexible production of a range of coloured powder coatings with a range of different reduced-gloss and other aesthetic effects is described in EP 539385 A.

Gloss reduction is achieved, for example, by adding uncoloured incompatible

25 particles of mean particle size $< 5\mu\text{m}$, or initially compatible particles of mean particle size $< 20\mu\text{m}$ of a polymer having a different functionality from the polymer of the main

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film-forming component. Amounts of the gloss-reducing agent are, for example, 5 or 10% by weight, although amounts up to 40% by weight are also disclosed.

SUMMARY OF THE INVENTION

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The present invention provides a powder coating composition in which powder particles are an agglomerate of individual particulate components fused or bonded together into composite particles, wherein the individual particulate components comprise

- 10 (1) one or more coloured film-forming base components having a Dv.99 of no more than 30 μ m, and
- (2) one or more uncoloured film-forming components, wherein at least one component (2a)
- (i) has a Dv.99 that is more than 20 μ m and
- 15 (ii) has a higher Dv.99 or higher Dv.50 than component (1) or, when there is more than one such component, than those components taken together, the ratio of coloured film-forming base component(s) to uncoloured film-forming component(s) in the composition being in the range of from 1:99 to 60:40 by weight.

As will be understood in the art, the volume percentiles Dv.x indicate for a

20 stated particle size (D) the percentage (x) of the total volume of the particles that lies below the stated particle size; the percentage (100-x) of the total volume lies at or above the stated size. Thus, for instance, Dv.50 is the median particle size of the sample, and on a particle size distribution graph Dv.99 is the point on the curve read along the particle size axis where the area under the curve below this particle size

25 represents 99% by volume of the particles. Thus, Dv.99 = 30 μ m indicates that 99% of the particles are below 30 μ m (but are not below 29 μ m). (For the avoidance of doubt, it

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should be noted that *all* particle sizes quoted herein are by volume.) Volume percentiles are measurable by laser diffraction techniques, for example by the Malvern Mastersizer.

Surprisingly, even with a high proportion of uncoloured component of significantly larger particle size than the coloured base components (whether judged according to Dv.99 or according to Dv.50), nevertheless the particles of the larger-sized component are not visible to the naked eye, so that the composition gives the appearance of a single colour.

A coloured base component comprises colouring material and film-forming polymer. Thus, for example, it may be constituted as a powder coating composition in its own right, containing the usual powder coating additives, but having the specified (reduced) particle size. Usually there will be at least two coloured base components in the composition, each having a Dv.99 of no more than 30µm.

An uncoloured film-forming component is usually also a powder coating composition in its own right, but having the specified particle size; there should be at least one uncoloured film-forming component having a higher Dv.99 and/or a higher Dv.50 than a coloured film-forming base component. (Usually, a component having a higher Dv.99 than another will also have a higher Dv.50 and *vice-versa*) Usually, there are two or more coloured film-forming base components each having a Dv.99 of no more than 30µm and at least one uncoloured film-forming component having a Dv.99 that is more than 20µm and that is higher than the Dv.99 of the coloured film-forming base components taken together (or having a Dv.99 >20µm and a Dv.50 that is higher than the Dv.50 of the coloured film-forming base components taken together). Very often that uncoloured film-forming component will have a higher Dv.99 (or a higher Dv.50) than each coloured film-forming base component. Preferably the uncoloured film-forming component has a Dv.99 of at least 40µm, for example at least 50µm, or

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more than 55 μ m, e.g. in the range of from 50 to 65 μ m. Preferably it will have a Dv.90 of no more than 75 μ m and advantageously will have a Dv.50 of at least 8 μ m, especially in the range of from 12 to 30 μ m. Such uncoloured film-forming components have the advantage of lower manufacturing cost in relation to the small-sized coloured components and their use allows easy adjustment of the polymer/ pigment ratio in the composition.

The present invention also provides a kit comprising the following separate components for agglomerating into powder coating compositions for the preparation of powder coatings in a number of different finishes:

- 10 • a plurality of coloured film-forming base components, each with a Dv.99 of no more than 30 μ m, and
- one or more uncoloured film-forming components, at least one having a higher Dv.99 or Dv.50 than each of the coloured film-forming components, and a Dv.99 that is more than 20 μ m, preferably more than 40 μ m and preferably no more than 90 μ m.

Such kits allow a rapid and flexible manufacture of a range of coloured powder coating compositions, reduced-gloss finishes being manufactured by the use of an uncoloured component that is incompatible with the coloured base component or that becomes incompatible therewith during film-formation.

20 The present invention also provides a powder coating composition comprising a non-agglomerated mixture of the individual particulate components specified above in the specified proportions.

**DETAILED DESCRIPTION OF THE INVENTION AND DESCRIPTION OF
PREFERRED EMBODIMENTS**

The individual particulate components may comprise, for example,

- 5 (1) one or more, usually two or more, coloured film-forming base components each
 having a Dv.99 of no more than 30 μ m, in an amount of from 1 to 60% by weight
 of the total film-forming components, and
- (2)(a) one or more uncoloured film-forming components each having a Dv.99 of more
 than 20 μ m and each having a higher Dv.99 (or a higher Dv.50) than the
10 coloured film-forming base component (1) or, when there is more than one such
 component, than those components taken together, in an amount of from 10 to
 99% by weight of the total film-forming components,
 and, if desired,
- (b) one or more other uncoloured film-forming components, in an amount of up to
15 30% by weight of the total film-forming components,

Where there is one uncoloured film-forming component (2a) this preferably has
a Dv.99 of up to 90 μ m, and where there are two or more uncoloured film-forming
components (2a) preferably at least one, and often all, such components have a Dv.99
of up to 90 μ m.

- 20 More especially, the present invention provides a powder coating composition,
suitable for providing a coating having certain appearance or performance attributes,
which comprises composite particles formed by the agglomeration of individual
particulate components fused or bonded together into composite particles such that the
composite particles are air-fluidisable and can be applied to a substrate by electrostatic
25 spray without causing the individual particles in the composite particles to break down

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under the mechanical and/or electrostatic forces associated with their application to a substrate, wherein the individual particulate components comprise

- (1) one or more, usually two or more, coloured film-forming base components each having a Dv.99 of no more than 30µm and
- 5 (2)(a) one or more uncoloured film-forming components each having a Dv.99 of more than 20µm and each having a higher Dv.99 or Dv.50 than the coloured film-forming base component (1) or, when there is more than one such component, than those components taken together,

and, if desired,

- 10 (b) one or more other uncoloured film-forming components, the ratio of coloured film-forming base component(s) to uncoloured film-forming component(s) in the composition being in the range of from 1:99 to 60:40 by weight, each particle of each film-forming component comprising a solid polymeric binder system at least a portion of which is a film-forming resin, the resin in the composition
- 15 being in an amount sufficient to impart film-forming properties to the composition.

Ratios of coloured film-forming component(s) to uncoloured film-forming component(s) in the composition of from 1:99, e.g. from 2:98, preferably from 5:95, and up to 60:40, e.g. no more than 50:50, advantageously no more than 40:60 and preferably no more than 30:70, should especially be mentioned.

- 20 Advantageously, the minimum weight of uncoloured film-forming component(s) (2a) corresponds to a ratio of coloured film-forming base component(s) (1) to uncoloured film-forming component(s) (2a) of 5:2. Preferably the weight of uncoloured film-forming component(s) (2a) is at least that of coloured film-forming component(s) (1) and, preferably, the weight of uncoloured film-forming component(s) (2a) is at least
- 25 that of other uncoloured film-forming component(s). Preferably the weight of

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uncoloured film-forming component(s) (2a) is at least that of other film-forming component(s) (1) and (2b) together.

In one embodiment, the uncoloured film-forming component(s) (2a) have a Dv.99 of more than 20 μ m and up to 40 μ m, the ratio of coloured film-forming base component(s) to uncoloured film-forming component(s) in the composition being in the range of from 1:99 to 30:70, for example from 2:98 to 30:70, by weight.

In another embodiment, the uncoloured film-forming component(s) have a Dv.99 of more than 40 μ m and preferably no more than 90 μ m, the ratio of coloured film-forming base component(s) to uncoloured film-forming component(s) in the composition being in the range of from 1:99 to 60:40, for example from 2:98 to 30:70, by weight.

Thus, the coloured film-forming base component(s) (1) may be, for example, at least 2%, for example at least 5%, and, for example, no more than 50%, advantageously no more than 40% and preferably no more than 30%, by weight of the total film-forming components. A content of coloured film-forming base component(s) of no more than 20%, for example from 10 to 20%, by weight of the total film-forming components should especially be mentioned.

The uncoloured film-forming component(s) (2) may be, for example, at least 10%, preferably at least 20%, more preferably at least 30%, especially at least 40%, more especially at least 50%, advantageously at least 60%, for example at least 70%, and, for example, up to 95%, by weight of the total film-forming components. A content of uncoloured film-forming component(s) of up to 90%, for example from 80 to 90%, by weight of the total film-forming components should be mentioned.

The uncoloured film-forming component(s) (2a) may be, for example, at least 10%, preferably at least 20%, more preferably at least 30%, especially at least 40%,

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more especially at least 50%, advantageously at least 60%, for example at least 70%, and for example up to 95%, by weight of the total film-forming components.

Where the composition also includes, as particulate component in the agglomerate, a further uncoloured film-forming component (component (2b)), there
5 may, for example, be no more than 30% by weight, calculated on all of the film-forming components together, of component(s) (2b) having (i) a Dv.99 that is $\leq 20\mu\text{m}$, and (ii) a Dv.99 (or Dv.50) that is no higher than the Dv.99 (or Dv.50 respectively) of the coloured film-forming component or of all the coloured film-forming components in the composition taken together. A content of uncoloured film-forming component(s) (2b) of
10 no more than 15%, for example 10% by weight or less, calculated on the weight of the total film-forming components should especially be mentioned.

In comparison with agglomerated coloured powder coating compositions described in EP 372860 A and EP 539385 A, compositions of the present invention contain a high proportion of uncoloured film-forming component, and the individual
15 coloured components necessarily contain a significantly higher content of pigment. Moreover, the particle size of the uncoloured particles in component(s) (2a) can be significantly larger than those of the coloured base component(s), without, surprisingly, affecting visual homogeneity. Thus, contrary to expectation and contrary to the suggestions in EP 372860 A and EP 539385 A, powders containing significant
20 quantities of uncoloured component(s) having, for example, a Dv.99 $> 40\mu\text{m}$ can be used to produce powder coating films in which the differences between the coloured particles and the uncoloured particles are not discernable by the unaided human eye. Maximising the level of larger-sized uncoloured component(s) will give cost advantages.

25 If desired, the composition may include as particulate component in the agglomerate as well as coloured film-forming base component(s) (1) and uncoloured

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film-forming component(s) (2a) and optionally (2b), one or more non-film-forming components, e.g. a texturing agent, a metallic or mica pigment, or a non-film-forming performance component. If desired, a non-film-forming component may be pre-mixed with a film-forming component, e.g. with an uncoloured film-forming component, to
5 form a masterbatch before mixing with the remaining components and then agglomerating. Alternatively, for example, a non-film-forming additive may be mixed with an uncoloured film-forming composition in an extruder and then micronised, to give an uncoloured film-forming component (2a) or (2b), depending on particle size, that also contains the desired aesthetic or performance additive.

10 A film-forming particulate component for inclusion in the agglomerate may itself be in the form of an agglomerate. Usually such a component would be formed by agglomeration of an uncoloured film-forming component with a non-film-forming component, for example a texturing additive or metallic or mica pigment.

Each film-forming component of the composition comprises at least one solid
15 film-forming resin and includes any curing agent required therefor, and is usually formed by an extrusion process and comminution to the requisite particle size. Where a film-forming component is coloured, the colouring agent or agents (pigments and/or dyes) is (are) generally extruded with the film-forming resin(s), plus any curing agent, so that particles formed therefrom comprise film-forming resin, colouring agent and,
20 where applicable, curing agent.

Reduction of gloss, for example to satin gloss (55-65% gloss) or matt (<30% gloss) or some other level, may be achieved by creating a surface which is rough on a microscopic scale using incompatible components or components that generate incompatibility. Film-forming components of similar chemistry but different gel times
25 provide incompatibility during film-formation, and reduction in gloss may be achieved by such means. Usually two (or more) film-forming base components are compatible with each other, but there may be an incompatible uncoloured film-forming component

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present. For example, there may be an uncoloured film-forming component having a different functionality from the coloured film-forming base component(s) and optionally also containing a different catalyst (both of which lead to different gel times). For example, coloured and uncoloured components may be based on polyesters of different functionality. For polyurethane systems using hydroxy-functional polyesters cured with an isocyanate (typically isophorone diisocyanate), hydroxy-functional polyesters with radically different functionality may be used, e.g. a hydroxy-functional polyester with a functionality of 7 for an uncoloured component and one with a functionality of 2 used for the coloured base component(s). Another possibility is to employ polymeric materials that are *per se* incompatible with each other, for example a polyester and an acrylic polymer.

In contrast to conventional prior art gloss-reduction processes, which generally use 50:50 non-fused mixtures of same-sized powders, with fused or bonded compositions of the present invention good gloss reduction can be achieved with substantially different proportions of gloss-reducing additive. The agglomerated material also does not suffer from particle segregation in the solid state as would dry-blended product, thus giving uniformity of product even after transportation and spraying.

Thus, uncoloured components can be used for extension of product ranges, to give different finishes. Also, by using different chemistries, they may be used to give different performance characteristics. The different chemistries may arise, for example, from the use of different film-forming polymers, e.g. polyester and acrylic or polyester and epoxy, but may also arise from the use of different curing agents, e.g. polyester with an epoxy curing agent in one component and polyester with a bis(beta-hydroxyalkylamide) curing agent such as PRIMID in another component.

In addition, or alternatively, an uncoloured film-forming component of the composition of the present invention may be compatible with the coloured film-forming

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base component(s). Usually all the coloured film-forming base components are compatible with one another.

An uncoloured film-forming component of a kit of the invention may be a pre-prepared uncoloured coating composition of the specified particle size or one of conventional size which is reduced in size just prior to use. Advantageously, for any particular type of film-forming chemistry (e.g. acid-functional polyester, hydroxy-functional polyester), a kit of the invention includes a "universal" gloss-reducing component suitable for all powder coating compositions of that chemistry. The present invention has the advantage of reducing costs while also reducing stocking levels and manufacturing capacity. It enables a very rapid and flexible service to be provided cheaply to the customer, allowing for the possibility of providing small quantities of powder coating compositions economically on request.

Advantageously, the coloured film-forming base components taken together contain at least 5%, e.g. at least 10%, and generally no more than 70% or 75%, e.g. no more than 60%, for example 20 to 40%, by weight of pigment, calculated on the total weight of these components. Advantageously, each contains at least 8% by weight of pigment, calculated on the weight of that component. The number of coloured film-forming base components in a kit may be, for example, at least 7, e.g. in the range of from 7 to 30.

Examples of pigments which may be used in the coloured base components are inorganic pigments, such as, for example, titanium dioxide white, red and yellow iron oxides, chrome pigments and carbon black, and organic pigments such as, for example, phthalocyanine, azo, anthraquinone, thioindigo, isodibenzanthrone, triphendioxane and quinacridone pigments, vat dye pigments and lakes of acid, basic and mordant dyestuffs. Dyes may be used instead of or as well as pigments. Each coloured base component of the coating composition may contain a single colorant

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(pigment or dye) or may contain more than one colorant. Where appropriate, a filler may be used to assist opacity, whilst minimising costs.

Additional pigment may alternatively be added as a separate component prior to agglomerating, especially if the pigment is close in colour to the mixed coloured film-forming base components. Any pigment added in this way would generally be no more than 3%, preferably up to 1%, by weight, based on the weight of the total composition, although amounts up to 5% may also be possible. Thus, for example, pigment in an amount of no more than 3% by weight, more especially up to 1% by weight, may be used to displace the colour of the components over a small colour region, this being used for colour tinting or colour correction of a batch.

Preferably, the total weight of pigment in the composition is at least 0.5%, more especially at least 5%, and preferably no more than 30%, although an amount up to 50% is potentially also possible.

One or more other separate components (3) may also be present. Other optional components include, for example, performance and aesthetic additives mentioned in EP 539385 A. Those components may, if desired, be pre-mixed with another component, for example an uncoloured film-forming component, with the components remaining as distinct components, e.g. (2a) and (3), before final agglomeration. Alternatively, the additives may be combined in a masterbatch with uncoloured film-forming polymer, often itself constituted as a powder coating composition in its own right, the masterbatch being prepared, for example, by co-extrusion of polymer and additive, followed by comminution, or by agglomeration of the particulate additive with uncoloured film-forming powder, to form uncoloured film-forming component (2a) or (2b), often (2a). Such further aesthetics additives may be present for example in an amount of from 0.5 to 50% by weight of the total composition. A non-film-forming performance additive is generally present in an amount of no more than 5% by weight of the composition, e.g. in an amount of from 0.5

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to 5% by weight. Where other component(s) are present in a composition of the present invention, the percentages of the specified coloured film-forming base component(s) and/or the specified uncoloured film-forming component(s) in the composition may be altered accordingly, but the ratio of coloured film-forming base component(s) to uncoloured film-forming component(s) will generally remain the same.

A composition of the present invention may contain, for example, at least 1%, e.g. at least 2%, often at least 5%, by weight of the specified coloured film-forming base component(s). Often the composition will contain at least 20%, e.g. at least 30% or at least 40%, by weight of the uncoloured film-forming component (2a) of the size specified above. Preferably, the content of uncoloured film-forming component(s) in the composition is at least 40%, e.g. at least 50%, and advantageously at least 60%, and preferably at least 70%, by weight. Amounts of at least 40% e.g. at least 50%, and advantageously at least 60%, and preferably at least 70%, by weight of uncoloured film-forming component(s) (2a) of the size specified above should especially be mentioned.

Ratios of from 1:99, e.g. from 2:98, preferably from 5:95, and up to 60:40, e.g. up to 50:50, advantageously up to 40:60 and preferably up to 30:70, for the ratio of coloured film-forming base component(s) (1) to uncoloured film-forming component(s) of the specified size (2a) should especially be mentioned.

Preferably, in each of the coloured film-forming base components all the component particles are $<25\mu\text{m}$. Advantageously the coloured film-forming base components have at least 90% by volume of particles < 20 microns, more especially at least 90% by volume < 10 microns, and advantageously the components have a $Dv.99$ of at least $6\mu\text{m}$, advantageously up to $25\mu\text{m}$. Advantageously, the $Dv.50$ of each such component is up to $18\mu\text{m}$, preferably up to $15\mu\text{m}$, e.g. up to $12\mu\text{m}$, advantageously at

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least 2 μ m, for example within the range of for example 2 to 8 μ m, preferably 2 to 6 μ m or 8 to 12 μ m; Dv.50 values $\geq 2\mu$ m and $\leq 5\mu$ m should especially be mentioned.

A coloured film-forming base component of a kit of the invention may, however, be of larger particle size and then reduced in size just prior to use. Accordingly, the present invention also provides a kit comprising the following separate components for agglomerating into powder coating compositions for the preparation of powder coatings in a number of different colours:

- at least 7 differently coloured film-forming base components,
- an uncoloured film-forming component that is compatible with the coloured film-forming base components and remains compatible therewith during film-formation and that has a Dv.99 of more than 40 μ m and preferably of no more than 90 μ m, and
- an uncoloured film-forming component that is incompatible with the coloured film-forming base components or that becomes incompatible therewith during film-formation and that has a Dv.99 of more than 40 μ m and preferably of no more than 90 μ m.

In one embodiment of the present invention, the individual particulate components of the powder coating composition comprise

- two or more coloured film-forming base components having a Dv.99 of no more than 30 μ m, and
 - one or more uncoloured film-forming components, at least one component having a higher Dv.99 or higher Dv.50 than at least one, preferably all, of the coloured film-forming base component(s), and having a Dv.99 of more than 20 μ m and preferably no more than 90 μ m,
- the ratio of coloured film-forming base components to uncoloured film-forming component(s) of the specified size being in the range of from 1:99 to 30:70 by weight.

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In a further embodiment of the present invention, the individual particulate components of the powder coating composition comprise

- two or more coloured film-forming base components having a Dv.99 of no more than 30µm, and
 - 5 • one or more uncoloured film-forming components, at least one component having a Dv.99 of more than 40µm and preferably no more than 90µm, the ratio of coloured film-forming base components to uncoloured film-forming component(s) of the specified size being in the range of from 1:99 to 60:40 by weight.
- 10 Preferably, the uncoloured film-forming component (2a) or at least one, and advantageously each, of the uncoloured film-forming components (2a) has a Dv.99 of at least 30µm, more especially at least 35µm, and advantageously at least 40µm. An uncoloured film-forming component having a Dv.50 of at least 8µm and up to 35µm, e.g. up to 30µm, and/or having a Dv.90 of at least 14µm should especially be
- 15 mentioned. An uncoloured film-forming component (2a) having a Dv.50 of at least 10µm and up to 35µm, e.g. in the range of from 12 to 30µm, and/or having a Dv.90 of at least 18µm and one having a Dv.90 of no more than 75µm should also especially be mentioned.

Uncoloured component(s) (2a) may, for example, have a Dv.99 or a Dv.50 that

20 is at least twice, e.g. at least three times, the Dv.99 or Dv.50 figure of the coloured component(s) (1) taken together. For example, the Dv.99 of component(s) (2a) may be at least 20µm, e.g. at least 30µm, more than that of component or components (1) taken together.

A powder coating composition of the invention will in general be a thermosetting

25 system, although thermoplastic systems (based, for example, on polyamides) can in principle be used instead.

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When a thermosetting resin is used, the solid polymeric binder system generally includes a solid curing agent for the thermosetting resin; alternatively two co-reactive film-forming thermosetting resins may be used. Thus, a thermosetting powder coating composition according to the invention may contain one or more film-forming polymers
5 selected from carboxy-functional polyester resins, hydroxy-functional polyester resins, epoxy resins, and functional acrylic resins. Carboxy-functional polyester resins should especially be mentioned.

A carboxy-functional polyester film-forming resin may be used, for example, with a polyepoxide curing agent. Such carboxy-functional polyester systems are
10 currently the most widely used powder coatings materials. The polyester generally has an acid value in the range 10-100, a number average molecular weight M_n of 1,500 to 10,000 and a glass transition temperature T_g of from 30°C to 85°C, preferably at least 40°C. The poly-epoxide can, for example, be a low molecular weight epoxy compound such as triglycidyl isocyanurate (TGIC), a compound such as diglycidyl terephthalate
15 condensed glycidyl ether of bisphenol A or a light-stable epoxy resin. Such a carboxy-functional polyester film-forming resin can alternatively be used with a bis(beta-hydroxyalkylamide) curing agent such as tetrakis(2-hydroxyethyl) adipamide.

Alternatively, a hydroxy-functional polyester can be used with a blocked isocyanate-functional curing agent or an amine-formaldehyde condensate such as, for
20 example, a melamine resin, a urea-formaldehyde resin, or a glycol ural formaldehyde resin, for example the material "Powderlink 1174" supplied by the Cyanamid Company, or hexahydroxymethyl melamine. A blocked isocyanate curing agent for a hydroxy-functional polyester may, for example, be internally blocked, such as the uret dione type, or may be of the caprolactam-blocked type, for example isopherone diisocyanate.

25 As a further possibility, an epoxy resin can be used with an amine-functional curing agent such as, for example, dicyandiamide. Instead of an amine-functional

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curing agent for an epoxy resin, a phenolic material may be used, preferably a material formed by reaction of epichlorohydrin with an excess of bisphenol A (that is to say, a polyphenol made by adducting bisphenol A and an epoxy resin). A functional acrylic resin, for example a carboxy-, hydroxy- or epoxy-functional resin can be used with an
5 appropriate curing agent.

Mixtures of film-forming polymers can be used; for example a carboxy-functional polyester can be used with a carboxy-functional acrylic resin and a curing agent such as a bis(beta-hydroxyalkylamide) which serves to cure both polymers. As further possibilities, for mixed binder systems, a carboxy-, hydroxy- or epoxy-functional
10 acrylic resin may be used with an epoxy resin or a polyester resin (carboxy- or hydroxy-functional). Such resin combinations may be selected so as to be co-curing, for example a carboxy-functional acrylic resin co-cured with an epoxy resin, or a carboxy-functional polyester co-cured with a glycidyl-functional acrylic resin. More usually, however, such mixed binder systems are formulated so as to be cured with a single
15 curing agent (for example, use of a blocked isocyanate to cure a hydroxy-functional acrylic resin and a hydroxy-functional polyester). Another preferred formulation involves the use of a different curing agent for each binder of a mixture of two polymeric binders (for example, an amine-cured epoxy resin used in conjunction with a blocked isocyanate-cured hydroxy-functional acrylic resin).

20 Other film-forming polymers which may be mentioned include functional fluoropolymers, functional fluorochloropolymers and functional fluoroacrylic polymers, each of which may be hydroxy-functional or carboxy-functional, and may be used as the sole film-forming polymer or in conjunction with one or more functional acrylic, polyester and/or epoxy resins, with appropriate curing agents for the functional
25 polymers.

Other curing agents which may be mentioned include epoxy phenol novolacs and epoxy cresol novolacs; isocyanate curing agents blocked with oximes, such as

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isophorone diisocyanate blocked with methyl ethyl ketoxime, tetramethylene xylene diisocyanate blocked with acetone oxime, and Desmodur W (dicyclohexylmethane diisocyanate curing agent) blocked with methyl ethyl ketoxime; light-stable epoxy resins such as "Santolink LSE 120" supplied by Monsanto; and alicyclic poly-epoxides
5 such as "EHPE-3150" supplied by Daicel.

The function of coatings is of course protective, but appearance is also important, and the film-forming resin and other ingredients are selected so as to provide the desired performance and appearance characteristics. In relation to performance, coatings should generally be durable and exhibit good weatherability,
10 stain or dirt resistance, chemical or solvent resistance and/or corrosion resistance, as well as good mechanical properties, e.g. hardness, flexibility or resistance to mechanical impact; the precise characteristics required will depend on the intended use. The composition must, of course, be capable of forming a coherent film on the substrate, and good flow and levelling of the composition on the substrate are required.
15 Accordingly, the powder coating composition generally also contains one or more performance additives such as, for example, a flow-promoting agent, a plasticiser, a stabiliser, for example a stabiliser against UV degradation, an anti-gassing agent, such as benzoin, or a filler. Such additives are known and standard additives for use in powder coating compositions. Usually, these performance additives will be
20 incorporated in any film-forming component before and/or during the extrusion or other homogenisation process, although, if appropriate, any such additive may alternatively be incorporated as a separate component in the agglomeration process.

Mixing and agglomeration methods are described in EP 372860 A and EP 539385 A.

25 The agglomerate may, for example, be prepared by mechanofusion of a mixture of the individual components, for example by mechanofusion at a temperature in the range of from 60 to 80°C, or by granulation using methanol or other suitable solvent as

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granulating agent, to produce composite particles that constitute a free-flowing and fluidisable powder.

Good fluidity of the powder is required for purposes of application to the substrate. This fluidity of powders is governed by their particle size, and particle size
5 also controls the application efficiency of a powder; powders with small particles, i.e. significant quantities <10 microns, more especially <5 microns, exhibit poor fluidity and application characteristics.

The present invention also provides a process for the preparation of a powder coating composition of the present invention, which comprises providing, in the
10 specified proportions, the specified one or more coloured film-forming base components and the one or more specified uncoloured film-forming components, and if desired one or more other uncoloured film-forming components and/or one or more non-film-forming components, and mixing and agglomerating the components such that the composition is air-fluidisable and can be applied to a substrate by electrostatic
15 spray.

Agglomeration prevents segregation of the constituents during application and handling, which otherwise would occur, for example during the application process itself (because of differential electrostatic charging) or in the attendant recovery and recycling process (because of differences in particle size and/or particle density) or in
20 transport, causing batch-to-batch variability in the resulting coating.

The composite particles produced may be likened to raspberries with the individual particles of the raspberry (the drupels) bonded to one another, although the "drupels" are of different sizes, and there will of course also be "raspberries" of different composition and different sizes in the powder as a whole. Inspection of a fused
25 agglomerated powder under an electron microscope shows that one particle is bonded to another and that the individual particles in the composites are more rounded than prior to agglomeration. When a conventional powder coating composition is inspected

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under an electron microscope, however, the powder particles are seen to be sharp-edged or angular, and are seen as separate, distinct particles - they are not fused to one another.

Furthermore, unlike conventional uniformly coloured powder coating compositions, that contain particles of only a single colour (produced by fusion in the melt extruder), powder coating compositions of this invention consist of a mixture of differently coloured particles and uncoloured particles but nevertheless give the appearance of a single colour on application to a substrate.

An agglomerated powder coating composition according to the invention may in principle be applied to a substrate by any suitable process of powder coating technology, for example by electrostatic spray coating, or by fluidised-bed or electrostatic fluidised-bed processes.

After application of the powder coating composition to a substrate, conversion of the resulting adherent particles into a continuous coating (including, where appropriate, curing of the applied composition) may be effected by heat treatment and/or by radiant energy, notably infra-red, ultra-violet or electron beam radiation.

The powder is usually cured on the substrate by the application of heat (the process of stoving), usually for a period of from 5 to 30 minutes and usually at a temperature in the range of from 150 to 220°C, although temperatures down to 90°C may be used for some resins, especially epoxy resins; the powder particles melt and flow and a film is formed. The curing times and temperatures are interdependent in accordance with the composition formulation that is used, and the following typical ranges may be mentioned:

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<u>Temperature/°C</u>	<u>Time</u>
280 to 100*	10 s to 40 min
250 to 150	15 s to 30 min
220 to 160	5 min to 20 min

- 5 * Temperature down to 90°C may be used for some resins, especially certain epoxy resins.

The invention also provides a process for forming a coating on a substrate, which comprises applying an agglomerated composition according to the invention to a substrate, for example by an electrostatic spray coating process, and heating the
10 applied composition to melt and fuse the particles and where appropriate cure the coating.

The film may be any suitable thickness. For decorative finishes, film thicknesses as low as 20 microns should be mentioned, but it is more usual for the film thickness to fall within the range 25-120 microns, with common ranges being 30-80
15 microns for some applications, and 60-120 microns or, more preferably, 60-100 microns for other applications, while film thicknesses of 80-150 microns are less common, but not rare.

The substrate may comprise a metal, a heat-stable plastics material, wood, glass, or a ceramic or textile material. Advantageously, a metal substrate is chemically
20 or mechanically cleaned prior to application of the composition, and is preferably subjected to chemical pre-treatment, for example with iron phosphate, zinc phosphate or chromate. Substrates other than metallic are in general preheated prior to application or, in the case of electrostatic spray application, are pretreated with a material that will aid such application.

25

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The following Examples illustrate the invention. In each case the particle sizes were measured on the Malvern Mastersizer X laser light-scattering device from Malvern Instruments.

5 EXAMPLES

Preparation of Individual Components

White, black and red coloured film-forming base components and different
10 uncoloured film-forming components were prepared by mixing the following formulations.

Component A - White Powder Coating Composition

15	Rutile titanium dioxide white pigment	600 g
	Carboxylic acid-functional polyester resin	360 g
	Bis(beta-hydroxyalkylamide) curing agent	13 g
	Benzoin degassing agent	4 g
	Flow modifiers	18 g
20	Surface waxes	5 g

Component B - Black Powder Coating Composition

	Carbon Black pigment	175 g
25	Carboxylic acid-functional polyester resin	772 g
	Bis(beta-hydroxyalkylamide) curing agent	27 g
	Benzoin degassing agent	4 g

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Flow modifiers	18 g
Surface waxes	4 g

Component C - Red Powder Coating Composition

5

Earth Red iron oxide pigment	125 g
Carboxylic acid-functional polyester resin	650 g
Bis(beta-hydroxyalkylamide) curing agent	24 g
Benzoin degassing agent	2 g
10 Flow modifiers	18 g
Surface waxes	4 g
Fillers (barytes)	177 g

For the coloured components A to C the ingredients were dry mixed and fed to
15 an extruder blender operating at a temperature of 100°C. The extruder produced a
sheet of pigmented resin which was ground to a particle size of below 100 µm and
milled on a 100 AFG jet-mill (manufacturer Hosakawa Micron) at 6 Bar grinding air
pressure and classified at a speed of 7000 rpm.

The particle size distribution for Components A, B and C was:

20

Dv.50 = 3.5µm

Dv.90 = 5.9µm

Dv.99 = 8.2µm

The polyester of Components A to C had an acid value of 18 to 30.

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Component D - Uncoloured Powder Coating Composition

	Carboxylic acid-functional polyester resin	650 g
	Bis(beta-hydroxyalkylamide) curing agent	24 g
5	Benzoin degassing agent	2 g
	Flow modifiers	18 g
	Surface waxes	4 g
	Fillers (barytes)	302 g

10 Component E - Uncoloured Powder Coating Composition for gloss-reduction

	Carboxylic acid-functional polyester resin	575 g
	Fillers (barytes)	333 g
	Benzoin degassing agent	4 g
15	Surface waxes	4 g
	Flow modifiers	18 g
	Bis(beta-hydroxyalkylamide) curing agent	65 g

For uncoloured components D and E the procedure for components A to C was
 20 repeated except that the jet-milling was carried out at 3000 rpm.

The particle size distribution for components D and E is:

$$Dv.50 = 18.4\mu m$$

$$Dv.90 = 36.2\mu m$$

$$Dv.99 = 51.0\mu m$$

25 The polyester of Component D had an acid value of 18 to 30 and the polyester
 of Component E had an acid value of 40 to 90.

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Component F - Uncoloured Powder Coating Composition for Texturing

	Carboxylic acid-functional polyester resin	780 g
5	Texturing agent: (PTFE wax, silicone wax, cellulose acetyl butyrate, ester modified polyether	220 g

The ingredients were dry mixed and fed to an extruder blender operating at a temperature of 100°C. This was ground to a powder in an air classified impact mill.

10 The particle size distribution for component F is

$$Dv.50 = 36\mu m$$

$$Dv.90 = 82\mu m$$

$$Dv.99 = 118\mu m$$

The polyester of Component F had an acid value of 18 to 30.

15

Component G - Uncoloured Powder Coating Composition for Pearlescent Effects

	Component E	800 g
	Mica Pigment (e.g. Iriodin 9111 supplied by Merck Ltd., Poole, Dorset, England)	200 g

The ingredients were blended together in a Henschel FM10 mixer for 30 minutes in total, taking the temperature to 54°C. The agglomerated powder was sieved through a 110µm steel mesh.

25 The particle size distribution for component G is

$$Dv.50 = 13\mu m$$

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Dv.90 = 24 μ mDv.99 = 38 μ mComponents H and I

5

Components A and B were prepared as before but milled on a 100 AFG jet-mill at 6 Bar grinding air pressure and classified at a speed of 12000rpm. These components were re-labelled Components H and I respectively.

The particle size distribution for Components H and I were:

10

Dv.50 = 2.6 μ mDv.90 = 5.3 μ mDv.99 = 6.4 μ mComponent J - Uncoloured Powder Coating composition for Tribo Application

15

Carboxylic acid-functional polyester resin	875 g
Bis-(beta-hydroxyalkylamide) curing agent	50 g
Benzoin degassing agent	2 g
Flow modifier	26 g
20 Tribostatic additives	47 g

The ingredients were dry mixed and fed to an extruder blender operating at a temperature of 100°C. The extruder produced a sheet of uncoloured resin which was ground to a particle size of below 100 μ m and milled on a 100 AFG jet-mill
25 (manufacturer Hosakawa Micron) at 6 Bar grinding air pressure and classified at a speed of 6500 rpm.

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The particle size distribution for Component J is

Dv.50 = 5.3 μ m

Dv.90 = 8.2 μ m

5 Dv.99 = 9.4 μ m

The polyester of component J had an acid value of 18 to 30.

Component K - Uncoloured Powder Coating Composition (Polyester/Epoxy)

10

Carboxylic acid-functional polyester resin 440 g

Glycidyl-functional Bisphenol-A epoxy resin

(type II or type III epoxy) 290 g

Benzoin degassing agent 2 g

15 Flow modifiers 18 g

Fillers (barytes) 250 g

The ingredients were dry mixed and fed to an extruder blender operating at a temperature of 100°C. This was ground to a powder in an air classified impact mill.

20

The particle size distribution for component K is

Dv.50 = 28 μ m

Dv.90 = 58 μ m

Dv.99 = 72 μ m

The polyester of Component K had an acid value of 18 to 30.

25

Preparation and Use of Agglomerated Powder Coating CompositionsExample 1

5 A mixture comprising:

Component A	187.5 g
Component B	16.7 g
Component C	100.0 g
Component D	695.8 g

10 was blended together in a Henschel FM10 mixture for 30 minutes in total, with a water jacket taking the temperature to 54°C. The agglomerated powder was sieved through a 110µm steel mesh and then electrostatically applied through a Gema PCG-1 corona spray gun onto an aluminium Q panel. This was then stoved at the recommended time and temperature.

15 A smooth, glossy coating that had a homogeneous dusky pink colour was produced.

Example 2

20 A mixture comprising

Component A	187.5 g
Component B	16.7 g
Component C	100.0 g
Component D	545.8 g
Component E	150.0 g

25 was agglomerated and applied to a substrate and stoved as in Example 1.

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As shown by their acid numbers, the polyester of Component E has a different functionality and hence different gel time from components A to D, and a smooth, matt coating of 30% gloss at 60° angle is produced that has a homogeneous dusky pink colour.

5

Example 3

A mixture comprising

	Component A	65 g
10	Component B	75 g
	Component C	80 g
	Component D	760 g
	Component F	20 g

was blended together in a Henschel mixer for 30 minutes in total, taking the
15 temperature to 54°C. The agglomerated powder was sieved through a 110µm steel mesh and then electrostatically applied through a Gema PCG-1 corona spray gun onto an aluminium Q Panel. This was then stoved at the recommended time and temperature.

A textured, glossy coating that had a homogeneous dark brown colour was
20 produced.

Example 4

A mixture comprising

25	Component A	250 g
	Component B	125 g

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Component D	475 g
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Component G	150 g
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was blended together in a Henschel mixer for 30 minutes in total, taking the temperature to 54°C. The agglomerated powder was sieved through a 110µm steel mesh and then electrostatically applied through a Gema PCG-1 corona spray gun onto an aluminium Q Panel. This was then stoved at the recommended time and temperature.

A smooth, matt coating that had a homogeneous grey colour and a pearlescent metallic effect was produced.

10

Example 5

A mixture comprising

Component H	40 g
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Component I	120 g
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Component D	670 g
-------------	-------

Component E	70 g
-------------	------

Component J	100 g
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was blended together in a Henschel mixer for 30 minutes in total, taking the temperature to 54°C. The agglomerated powder was sieved through a 110µm steel mesh and then electrostatically applied by a tribostatic gun onto an aluminium Q Panel. This was then stoved at the recommended time and temperature.

A smooth, satin coating that had a homogeneous charcoal colour was produced.

25

Example 6

A mixture comprising:

	Component A	187.5 g
5	Component B	16.7 g
	Component C	100.0 g
	Component K	695.8 g

was blended together in a Henschel FM10 mixture for 30 minutes in total, with a water jacket taking the temperature to 54°C. The agglomerated powder was sieved through
10 a 110µm steel mesh and then electrostatically applied through a Gema PCG-1 corona spray gun onto an aluminium Q panel. This was then stoved at the recommended time and temperature.

A smooth, glossy coating that had a homogeneous dusky pink colour was produced.

CLAIMS

1. A powder coating composition in which powder particles are an agglomerate of individual particulate components fused or bonded together into composite particles, wherein the individual particulate components comprise
- 5 (1) one or more coloured film-forming base components having a Dv.99 of no more than 30µm, and
- (2) one or more uncoloured film-forming components, wherein at least one component (2a) (i) has a Dv.99 that is more than 20µm and (ii) has a higher
- 10 Dv.99 or higher Dv.50 than component (1) or, when there is more than one coloured component, than those components taken together,
- the ratio of coloured film-forming base component(s) to uncoloured film-forming component(s) in the composition being in the range of from 1:99 to 60:40 by weight.
- 15 2. A powder coating composition as claimed in claim 1, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 10% by weight of the total film-forming components.
3. A powder coating composition as claimed in claim 1 or claim 2, wherein
- 20 there is no more than 30% by weight, calculated on the weight of the total film-forming components, of uncoloured film-forming component(s) having a Dv.99 (i) that is no higher than the Dv.99 of the coloured film-forming component or components taken together, and (ii) that is less than 20µm.

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4. A powder coating composition in which powder particles are an agglomerate of individual particulate components fused or bonded together into composite particles, wherein the individual particulate components comprise

(1) one or more coloured film-forming base components each having a Dv.99 of no more than 30µm, in an amount of from 1 to 60% by weight of the total film-forming components, and

(2)(a) one or more uncoloured film-forming components each having a Dv.99 of more than 20µm and each having a higher Dv.99 and/or a higher Dv.50 than the coloured film-forming base component (1) or, when there is more than one such component, than those components taken together, in an amount of from 10 to 99% by weight of the total film-forming components, and, if desired,

(b) one or more other uncoloured film-forming components, in an amount of up to 30% by weight of the total film-forming components.

5. A powder coating composition as claimed in any one of claims 1 to 4, wherein there are two or more coloured film-forming base components (1).

6. A powder coating composition in which powder particles are an agglomerate of individual particulate components fused or bonded together into composite particles, wherein the individual particulate components comprise

(1) two or more coloured film-forming base components having a Dv.99 of no more than 30µm, and

(2) one or more uncoloured film-forming components, at least one component (2a) having a Dv.99 of more than 20µm and that is higher than the Dv.99 of

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component (1) or, when there is more than one such component, of those components taken together,

the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2) in the composition being in the range of from 1:99 to 30:70 by weight.

5

7. A powder coating composition as claimed in claim 6, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 10% by weight of the total film-forming components.

10

8. A powder coating composition as claimed in claim 6 or claim 7, wherein there is no more than 30% by weight, calculated on the weight of the total film-forming components, of uncoloured film-forming component(s) having a Dv.99 (i) that is no higher than the Dv.99 of the coloured film-forming component or components taken together, and (ii) that is less than 20 μ m.

15

9. A powder coating composition as claimed in any one of claims 1 to 8, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components has a Dv.99 of at least 30 μ m.

20

10. A powder coating composition as claimed in claim 9, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components has a Dv.99 of at least 35 μ m.

25

11. A powder coating composition as claimed in claim 10, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components has a Dv.99 of at least 40 μ m.

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12. A powder coating composition in which powder particles are an agglomerate of individual particulate components fused or bonded together into composite particles, wherein the individual particulate components comprise

- 5 (1) two or more coloured film-forming base components having a Dv.99 of no more than 30 μ m, and
- (2) one or more uncoloured film-forming components, at least one component (2a) having a Dv.99 of more than 40 μ m,

the ratio of coloured film-forming base components to uncoloured film-forming
10 component(s) in the composition being in the range of from 1:99 to 60:40 by weight.

13. A powder coating composition as claimed in claim 12, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 10% by weight of the total film-forming components.

15

14. A powder coating composition as claimed in claim 12 or claim 13, wherein there is no more than 30% by weight, calculated on the weight of the total film-forming components, of uncoloured film-forming component(s) having a Dv.99 (i) that is no higher than the Dv.99 of the coloured film-forming component or components
20 taken together, and (ii) that is less than 20 μ m.

15. A powder coating composition as claimed in any one of claims 1 to 14, wherein the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2a) is in the range of from 1:99 to 50:50 by weight.

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16. A powder coating composition as claimed in claim 15, wherein the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2a) is in the range of from 1:99 to 40:60 by weight.

5 17. A powder coating composition as claimed in claim 16, wherein the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2a) is in the range of from 1:99 to 30:70 by weight.

10 18. A powder coating composition as claimed in any one of claims 1 to 17, wherein the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2a) is in the range of from 5:95 to 30:70.

15 19. A powder coating composition as claimed in any one of claims 1 to 18, wherein the uncoloured film-forming component or components (2) are present in an amount of at least 50% by weight of the total film-forming components.

20 20. A powder coating composition as claimed in claim 19, wherein the uncoloured film-forming component or components (2) are present in an amount of at least 60% by weight of the total film-forming components.

21. A powder coating composition as claimed in claim 20, wherein the uncoloured film-forming component or components (2) are present in an amount of at least 70% by weight of the total film-forming components.

25 22. A powder coating composition as claimed in any one of claims 2 to 21, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 20% by weight of the total film-forming components.

23. A powder coating composition as claimed in claim 22, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 30% by weight of the total film-forming components.

5

24. A powder coating composition as claimed in claim 23, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 40% by weight of the total film-forming components.

10

25. A powder coating composition as claimed in claim 24, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 50% by weight of the total film-forming components.

15

26. A powder coating composition as claimed in claim 25, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 60% by weight of the total film-forming components.

20

27. A powder coating composition as claimed in any one of claims 1 to 26, wherein there is no more than 15% by weight, calculated on the weight of total film-forming components, of uncoloured film-forming component(s) (2b).

28. A powder coating composition as claimed in any one of claims 1 to 24, wherein there are two or more compatible coloured film-forming base components (1).

25

29. A powder coating composition as claimed in any one of claims 1 to 28, wherein the uncoloured film-forming component (2a) or at least one of the uncoloured

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film-forming components listed under (2a) and (2b) is compatible with the coloured film-forming base components (1) during film-formation.

30. A powder coating composition as claimed in any one of claims 1 to 29,
5 wherein the uncoloured film-forming component (2a) or at least one of the uncoloured film-forming components listed under (2a) and (2b) is incompatible with the coloured film-forming base component(s) (1) or becomes incompatible therewith during film-formation.

10 31. A powder coating composition as claimed in any one of claims 1 to 30, wherein the coloured film-forming base component(s) (1) contain a polyester.

32. A powder coating composition as claimed in claim 30 and claim 31,
wherein the uncoloured film-forming component (2a) or at least one of the uncoloured
15 film-forming components listed under (2a) and (2b) contains a polyester having a different functionality from the polyester of the coloured film-forming base component(s) (1).

33. A powder coating composition as claimed in claim 31 or claim 32, which
20 includes an uncoloured film-forming component (2a) or (2b) containing a polyester, that component and the coloured film-forming base component(s) (1) containing different curing agents, one of those being an epoxy curing agent or a co-reactable epoxy resin.

34. A powder coating composition as claimed in any one of claims 1 to 33,
25 which includes an uncoloured film-forming component (2a) or (2b) which is itself an agglomerate of an uncoloured film-forming component fused or bonded to form composite particles with a non-film-forming component.

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35. A powder coating composition as claimed in any one of claims 1 to 34, wherein component (2a) or (2b) includes a texturing additive.

5 36. A powder coating composition as claimed in claim 34, wherein the agglomerated component (2a) or (2b) includes mica.

37. A powder coating composition as claimed in any one of claims 1 to 36, wherein the uncoloured film-forming component (2a) or at least one of the uncoloured
10 film-forming components (2a) has a Dv.99 of no more than 90µm.

38. A powder coating composition as claimed in any one of claims 1 to 37, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components (2a) has a Dv.90 of at least 14µm.
15

39. A powder coating composition as claimed in claim 38, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components (2a) has a Dv.90 of at least 18µm.

20 40. A powder coating composition as claimed in any one of claims 1 to 39, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components (2a) has a Dv.90 of no more than 75µm.

41. A powder coating composition as claimed in any one of claims 1 to 40,
25 wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components (2a) has a Dv.99 in the range of from 50 to 65µm.

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42. A powder coating composition as claimed in any one of claims 1 to 41, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components (2a) has a Dv.50 in the range of from 5 to 45 μ m.

5

43. A powder coating composition as claimed in claim 42, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components (2a) has a Dv.50 of at least 8 μ m.

10

44. A powder coating composition as claimed in claim 43, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components (2a) has a Dv.99 of at least 40 μ m and a Dv.50 of at least 10 μ m

15

45. A powder coating composition as claimed in claim 43 or claim 44, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components (2a) has a Dv.50 in the range of from 12 to 30 μ m.

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46. A powder coating composition as claimed in any one of claims 1 to 45, wherein the coloured film-forming base components or at least one of the coloured film-forming base components (1) have a Dv.99 in the range of from 6 to 25 μ m.

25

47. A powder coating composition as claimed in any one of claims 1 to 46, wherein the coloured film-forming base components or at least one of the coloured film-forming base components (1) have a Dv.50 of no more than 18 μ m.

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48. A powder coating composition as claimed in claim 47, wherein the coloured film-forming base components or at least one of the coloured film-forming base components (1) have a Dv.50 of no more than 15µm.

5 49. A powder coating composition as claimed in claim 48, wherein the coloured film-forming base components or at least one of the coloured film-forming base components (1) have a Dv.50 in the range of from 2 to 12µm.

50. A powder coating composition as claimed in any one of claims 1 to 49,
10 wherein the coloured film-forming base components contain in total from 5 to 70 weight % of pigment, calculated on the total weight of those components.

51. A powder coating composition as claimed in any one of claims 1 to 50,
wherein the coloured film-forming base components contain in total from 0.5 to 50
15 weight % of pigment, calculated on the total weight of the composition.

52. A powder coating composition as claimed in any one of claims 1 to 51,
wherein the individual particulate components of the agglomerate include one or more
non-film-forming component (3).
20

53. A powder coating composition as claimed in claim 52, wherein the individual particulate components of the agglomerate include a texturing agent (3).

54. A powder coating composition as claimed in claim 52 or claim 53,
25 wherein the non-film-forming component or components constitute up to 50% by weight of the total particulate components of the composition.



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55. A kit comprising the following separate particulate components for agglomerating into powder coating compositions for the preparation of powder coatings in a number of different colours:
- 5 • a plurality of differently coloured film-forming base components, each with a Dv.99 of no more than 30 μ m, and
 - one or more uncoloured film-forming components, each having a higher Dv.99, and/or a higher Dv.50, each Dv.99 being more than 40 μ m.
- 10 56. A kit as claimed in claim 55, wherein the uncoloured film-forming component or at least one of the uncoloured film-forming components has a Dv.99 of no more than 90 μ m.
- 15 57. A kit as claimed in claim 55 or claim 56, which includes at least 7 differently coloured film-forming base components.
- 20 58. A kit as claimed in any one of claims 55 to 57, which includes an uncoloured film-forming component that is compatible during film-formation with the coloured film-forming base components, and an uncoloured film-forming component that is incompatible with the coloured film-forming base components or that becomes incompatible therewith during film-formation.
- 25 59. A kit comprising the following separate particulate components for the manufacture of agglomerated powder coating compositions for the preparation of powder coatings in a number of different colours:
- at least 7 differently coloured film-forming base components,

- 45 -

- an uncoloured film-forming component that is compatible with the coloured film-forming base components and remains compatible during film-formation and that has a Dv.99 of more than 40 μ m and no more than 90 μ m, and
- an uncoloured film-forming component that is incompatible with the coloured film-forming base components or that becomes incompatible therewith during film-formation, and that has a Dv.99 of more than 40 μ m and no more than 90 μ m.

60. A kit as claimed in claim 59, which includes means for comminution of the coloured film-forming base components to a powder having Dv.99 of no more than 30 μ m.

61. A kit as claimed in any one of claims 55 to 60, wherein the different components are as specified in any one of claims 31 to 53.

62. A kit as claimed in any one of claims 55 to 61, which includes at least 3 uncoloured film-forming components.

63. A kit as claimed in any one of claims 55 to 62, which includes means for agglomerating the components to produce a fluidisable powder.

64. A process for the preparation of a powder coating composition as claimed in any one of claims 1 to 54, which comprises providing the specified one or more coloured film-forming base components (1) and the one or more specified uncoloured film-forming components (2a) and if desired one or more other components selected from other uncoloured film-forming components (2b) and non-film-forming components (3), in the specified proportions, and mixing and agglomerating the

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components into composite particles such that the composition is air-fluidisable and can be applied to a substrate by electrostatic spray.

65. A process for the preparation of a powder coating composition as
5 claimed in claim 1 from a kit comprising a plurality of differently coloured film-forming
base components and one or more uncoloured film-forming components having a
Dv.99 of more than 40 μ m, which comprises comminuting at least one of the coloured
film-forming base components to provide a powder having a Dv.99 of no more than
30 μ m, and mixing and agglomerating the comminuted coloured film-forming base
10 component(s) and at least one of the specified uncoloured film-forming components
having a Dv.99 or a Dv.50 higher than the Dv.99 or Dv.50 respectively of the
comminuted coloured film-forming base component or components taken together, in
the proportions specified in claim 1, to form composite particles, such that the
composition is air-fluidisable and can be applied to a substrate by electrostatic spray.

15

66. A powder coating composition when prepared by a process as claimed
in claim 64 or claim 65.

67. A process for forming a coating on a substrate, which comprises
20 applying an agglomerated composition as claimed in any one of claims 1 to 54 or claim
66 to a substrate, and heating the applied composition to form a continuous coating.

68. A substrate coated by a process as claimed in claim 67.

INTERNATIONAL SEARCH REPORT

International Application No

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A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 C09D5/03

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 C09D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WO 91 18951 A (COURTAULDS COATINGS) 12 December 1991 (1991-12-12) page 40, line 23 -page 43, line 5 page 52, line 20-24 page 53, line 19 -page 54, line 1 & EP 0 539 385 A cited in the application ---	1-68
A	EP 0 459 048 A (COURTAULDS COATINGS) 4 December 1991 (1991-12-04) page 3, line 20-39 ---	1, 6, 55, 59, 64-68
A	PATENT ABSTRACTS OF JAPAN vol. 012, no. 159 (C-495), 14 May 1988 (1988-05-14) & JP 62 270672 A (ASAHI CHEM IND CO LTD), 25 November 1987 (1987-11-25) abstract -----	



Further documents are listed in the continuation of box C.



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Information on patent family members

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(21) International Application Number: PCT/GB91/00868 (22) International Filing Date: 31 May 1991 (31.05.91) (30) Priority data: 9012315.9 1 June 1990 (01.06.90) GB (71) Applicant (for all designated States except US): COURTAULDS COATINGS (HOLDINGS) LIMITED [GB/GB]; 18 Hanover Square, London W1A 1AD (GB). (72) Inventors; and (75) Inventors/Applicants (for US only) : SINCLAIR-DAY, John, David [GB/GB]; 13 Jasper Avenue, Greenside, Ryton, Tyne & Wear NE40 4RS (GB). CASSIDY, Stephen, Paul [GB/GB]; 8 Birtley Close, Kingsmere, Gosforth, Newcastle upon Tyne NE3 4RL (GB). RING, John [GB/GB]; 26 Meadowvale, Darras Hall, Ponteland, Newcastle upon Tyne NE20 9NF (GB). CORDINER, Andrew, George [GB/GB]; 90 Benton Road, High Heaton, Newcastle upon Tyne NE7 7DX (GB).		(74) Agents: SENIOR, Janet et al.; Abel & Imray, Northumberland House, 303-306 High Holborn, London WC1V 7LH (GB). (81) Designated States: AT (European patent), AU, BE (European patent), BR, CA, CH (European patent), DE (European patent), DK (European patent), ES (European patent), FI, FR (European patent), GB (European patent), GR (European patent), HU, IT (European patent), JP, KR, LU (European patent), NL (European patent), NO, PL, SE (European patent), SU, US. Published <i>With international search report.</i> <i>Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>
(54) Title: POWDER COATING COMPOSITIONS (57) Abstract A composition of the present invention for application as a powder coating is in the form of a fused agglomerate of different particulate components consisting of a primary film-forming component and one or more other components selected from film-forming and non-film-forming components. The agglomerated composition may be used to introduce a variety of additives into powder coatings and to provide a variety of aesthetic effects, both in single-layer and multilayer systems.		

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Powder Coating Compositions

This invention relates to powder coatings.

Powder coatings generally comprise a solid film-
5 forming resin, usually with one or more pigments. They
can be thermoplastic but are more usually thermosetting,
incorporating two co-reactive film-forming resins or
incorporating a curing agent for the film-forming resin
in the powder particles.

10 Powder coatings are generally prepared by intimately
mixing the ingredients, for example in an extruder at a
temperature above the softening point of the film-forming
resin but below the curing temperature of the composition
(the process of extrusion), and comminuting the mixture
15 to the desired particle size in suitable grinding
equipment (the process of micronising).

The powder may be applied to the substrate by
various means, for example by the use of fluid beds, or
most commonly by electrostatic spray gun, and ideally the
20 particle size distribution required for most commercial
electrostatic spray apparatus is between 10 and 120 μ m,
with a mean particle size by volume within the range of
15-75 μ m. (All mean particle sizes quoted herein are by
volume.) Generally, the powders have at least 90% by
25 volume of particles between 20 μ m and 100 μ m and no more
than 70% < 50 μ m, and have a mean particle size at least

35 μ m, and generally no more than 60 μ m, often in the range of from 35 to 55 μ m, usually 35 to 50 μ m. In the electrostatic spray process the powder coating particles are electrostatically charged and the charged particles are attracted to the substrate which is earthed or oppositely charged. The powder coating which does not adhere to the substrate can be recovered for re-use, so that powder coatings are economical in use of ingredients as well as non-polluting to the environment. The powder is then cured on the substrate by the application of heat (the process of stoving) usually for a period of from 5 to 30 minutes and usually at a temperature in the range of from 150 to 220°C, although temperatures down to 120°C may be used for some resins, especially epoxy resins; the powder particles melt and flow and a film is formed.

Various different finishes, for example reduced gloss and textured finishes, may be obtained.

Reduction of gloss in the powder coating from full gloss (80-90% measured at a 60° viewing angle) to some other lower level, for example satin gloss (55-65% gloss) or matt (< 30% gloss), is achieved by creating a surface which is rough on a microscopic scale. This surface roughness must be sufficient to cause a reduction in the specular reflection from the film by scattering the incident light; if it is visible, however, a texturing effect is achieved in the film. In liquid paints this gloss reduction is usually achieved by the use of pigment

and/or filler particles at high volume concentrations. However, this technique cannot be used as the sole route to gloss reduction in powder coatings as a high content of filler particles would lead to too reduced a surface flow during curing.

The procedure used is to set up reactions within the curing film such that two different gelation rates are set up within the curing matrix. With acid-functional polyesters, a fast gelling (reacting) powder and a slow gelling powder may be manufactured separately and mixed after the micronising stage or, more usually, the components are mixed prior to micronising. The faster gelling domains form particles which disrupt the surface flow of the slower gelling portion of the matrix. For production simplicity and economics, a one-component matt is preferred, but the production of an adequate range of matt finishes using a one-component system is not possible in all resin types, and there is no single matting agent that can be used with all resin types to provide a wide variation of gloss levels.

For texture, there are a wide number of agents that can be added to powders to achieve different surface effects, acting by disrupting the flow of the polymer film. For a stippled finish, micronised PTFE (polytetrafluoroethylene) is used. For a wrinkle finish, cellulose acetate butyrate resin (CAB) or acrylate homo- and copolymers may be used; an example of the latter is

Acronal 4F (Trade Mark), which is usually added before extrusion as a flow aid, but which in micronised form is used for texturing. For a hammer finish (gross surface depressions), a metallic pigment and texturing agent are used. In addition, texturing agents based on high molecular weight thermoplastics are commonly added to thermoset powder coatings, giving rise to uniformly poor flow across the surface which manifests itself as a texture.

PTFE is preferably added to the premix before extrusion and is fully incorporated into the extrudate in order to minimise product variation through segregation. However, the micronised PTFE has to be prepared in a particular fashion to give batch-to-batch consistency.

CAB may be added to the finished powder or, since as a post-additive it is prone to segregation with use, preferably at the premix stage. It does not melt in the extruder, and the inhomogeneous dispersion thereby produced gives rise to the texture. Some texturing agents, however, for example Acronal 4F (T.M.), have to be added post-extrusion since the extrusion process would render them ineffective by mixing them intimately with the continuous phase of the coating system. Powders containing post-additives are susceptible to segregation which causes inconsistency in the texturing effect on application of the powder.

Multilayer coatings may be produced using mixed

polymer systems by stratification or "surface segregation" of incompatible phases during film formation. Mixtures of, for example, an acrylic polymer and polyester may be used to form a multilayer coating, with
5 the acrylic polymer migrating to the surface of the coating (the air interface) and the polyester forming the lower layer on the substrate. As compared with pure polyesters, the multilayer coating provides improved stain, solvent and UV resistance, for example resistance
10 to degradation by sunlight, and improved durability and weathering performance, and, as compared with pure acrylic, improved mechanical performance.

If powders are made by pre-mixing both the polymers prior to extruding, however, the stratification is not
15 uniform from formulation to formulation or from colour to colour, such that the improvements described cannot be guaranteed. If, alternatively, acrylic and polyester powder coating powders are mixed prior to application, stratification can be complicated by the formation of
20 textured films due to the incompatibility of the two polymer systems. The two powders will also be subject to problems of segregation of the powders in the solid state.

Our copending application GB 2226824 A describes a
25 colour mixing process for powder coatings in which sufficiently small-sized particles, < 20 μ m in size and advantageously < 10 μ m, are used that mixed colours

applied to a substrate have homogeneous appearance.

Before application to the substrate the mixture is generally subjected to a process of agglomeration in which the small-sized particles are fused into composite
5 particles, for example by mechanofusion, for example at a temperature in the range of from 60 to 80°C, and this converts the mixture from a cohesive mass to a free-flowing and fluidisable powder, which can be applied by conventional means. Agglomeration also prevents segrega-
10 tion of the constituents during application and handling, which is otherwise bound to occur, for example during the application process itself (because of differential electrostatic charging) or in the attendant recovery and recycling process (because of differences in particle
15 size and/or particle density) or in transport, causing batch-to-batch variability in the resulting coating.

The present invention is based on the realisation that formation of a fused or bonded agglomerate provides a suitable method, not only for colour mixing, but also
20 for the introduction of a variety of additives into powder coating compositions, both in single layer and multilayer systems.

The agglomeration process has had a number of advantages:

- 25 (i) Firstly, the agglomeration process provides an extension of our colour mixing process to give a range of aesthetic effects.

(ii) Secondly, it provides effectively a permanent fixing in the composition for known materials which would be prone to segregation in the solid state during the handling process, for example in transportation and application, and during recycling of over-sprayed particles.

Thus, more especially, it has led to the production of gloss-reduced and textured coatings which do not have the disadvantages described above of conventional such coatings.

(iii) Thirdly, with mixed polymer systems it facilitates enhancement or manipulation of segregation (stratification) within the film during film formation.

Thus, it has led to the production of more satisfactory multilayer coatings that do not have the above-mentioned disadvantages of the prior art systems.

(iv) Fourthly, incorporation of additives by agglomeration, rather than extrusion, provides the potential for the preparation of a variety of new products which could not be manufactured by conventional routes (e.g. extrusion and micronising), for example because the additive would be damaged by the manufacturing process, or would be likely itself to damage the process equipment.

25 Metallic pigments such as, for example, aluminium or 'gold bronze' flakes are used in powder coating to add lustre to the coating finish; the most common metallic

pigment used is aluminium. In a "leafing" system, the aluminium flakes orient themselves in a continuous layer at or near the surface of the film, producing an opaque silver finish. The pigments are usually incorporated by dry blending; a lustre effect, achieved by the pigment "leafing", for example, may easily be destroyed by strong shear forces, such as those found in extruders and micronisers. However, the loose metallic flakes can cause unwanted electrical discharge within the spray gun, and the presence of free metallic pigments within the powder(s) also represents a significant increase in explosion hazard.

These problems have been overcome by a special technique developed by Wolstenholme Bronze Powders Ltd.. The technique involves a mechanofusion or bonding of the individual flakes of metallic pigment to the surface of conventional powder coating particles; as soon as the powder begins to melt during stoving the metallic flakes are released and rise to the surface with the powder coating film, thereby producing a good leafing effect and a bright metallic finish. A range of hammer and other textured metallic finishes can be produced by using, in addition, an appropriate hammer or structure additive. In the review "Ten Years of Bonded Metallic Powder Coatings" by Keith S. Carter in Polymers Paint Colour Journal, Volume 176, No. 4179, November 1986, the author indicates that, although the bonding process is used

mainly with flaky metallic pigments, other pigments such as pearlescent pigments - which, like metallic pigments, should not be extruded and ground, and which give a special finish -can also be successfully bonded.

- 5 However, the technique has not previously been applied beyond the specific field of metallic or lustre finishes, and nor have there been any suggestions to do so.

Accordingly, the present invention provides a composition suitable for application as a powder coating
10 and which is in the form of a fused agglomerate of different particulate components, with the exception of the agglomerated composition claimed in GB 2226824 A and of the bonded metallic powder coatings described above.

A number of powder coating processes using combina-
15 tions of separate components have been proposed, generally with the aim of reducing blocking (clumping) in the powder on storage.

US Patent 4,260,066 (Celanese Corporation) describes powder coatings in which small tacky particles comprising
20 a melt flow modifier and adhesion promoter are adhered to non-tacky particles containing a thermoplastic elastomer, melt flow modifier, adhesion promoter and stabiliser, to form composite particles which do not agglomerate on storage.

25 Pending applications EP 0 250 183 A, EP 0 372 958 A and EP 0 389 080 A (Nippon Paint Company Limited) describ the addition of, respectively, cross-linked

polymer particles (usually microparticles), an anisotropic crystalline polymer (usually in the form of microparticles), and microparticles of comparatively high Tg to a base resin at any stage of preparation. The components may, for example, be combined during the mixing, milling, pulverising or sieving steps or, in a wet process, may be dispersed together in an appropriate solvent or may be combined in the subsequent spray-drying step.

However, in none of the Nippon Paint or Celanese Corporation processes described is the second component firmly fixed to the surface of the first component and resistant to separation by mechanical or electrostatic forces.

More especially, the present invention provides a composition suitable for application as a powder coating and which is in the form of a fused agglomerate of different particulate components, provided that,

- if the agglomerate contains a metallic or lustre component and a film-forming component of mean particle size 35 to 60 μ m and no more than 70% by volume < 50 μ m, it also contains an incompatible film-forming component or a non-film-forming performance component or two or more such components, and
- if the agglomerate contains two or more differently coloured compatible film-forming components and optionally an uncoloured compatible film-forming

component and the size of the particles in each of those film-forming components is sufficiently low that when the powder coating is applied to a substrate and heated to form a continuous coating the differences in colour in the cured powder coating arising from the different coloured and any uncoloured particles cannot be discerned by the human eye, it also contains an incompatible film-forming component or a non-film-forming component or two or more such components.

More especially, the present invention provides a composition suitable for application as a powder coating and which is in the form of a fused agglomerate of different particulate components, provided that,

- 15 - if the agglomerate contains a metallic or lustre component and a fluidisable film-forming component, it also contains an incompatible film-forming component or a non-film-forming performance component or two or more such components, and
- 20 - if the agglomerate contains two or more differently coloured compatible film-forming components and optionally an uncoloured compatible film-forming component and the size of the particles in each of those film-forming components is sufficiently low
- 25 that when the powder coating is applied to a substrate and heated to form a continuous coating the differences in colour in the cured powder

coating arising from the different coloured and any uncoloured particles cannot be discerned by the human eye, it also contains an incompatible film-forming component or a non-film-forming component or
5 two or more such components.

An agglomerate of the present invention contains one or more film-forming systems (polymeric binder systems) and usually contains also at least one colouring agent. A film-forming system itself comprises a solid
10 film-forming resin and any curing agent required therefor. (By a film-forming resin/polymer we mean one that acts as a binder, that is, that has the capability of wetting pigments and providing cohesive strength between pigment particles and that wets or binds to the
15 substrate, and that melts and flows in the curing/stoving process after application to the substrate to form a homogeneous film.) Usually any colouring agent or agents (pigments and/or dyes) and any curing agent is extruded with the or with one or more of the film-forming resins
20 so that particles formed therefrom comprise a film-forming resin and colouring agent or agents and/or curing agent; generally at least the majority of such particles contain at least one colouring agent. However, any colouring agent and any curing agent may each, if
25 desired, be present as a separate component. There may, if desired, be two or more film-forming components in the agglomerate; each may be coloured or uncoloured.

One or more other additives may, if desired, be contained in the agglomerate; each may be in a film-forming component or as a separate component (a non-film-forming component).

- 5 A non-film-forming additive, which may, if desired, be present as a separate component, may be one having an effect on performance (a "performance additive" or "functional additive"), and/or an aesthetic effect (an "aesthetics additive"), usually a visual effect (an
- 10 "appearance additive"). A performance additive may be one bringing about an effect on the resulting coating and/or on the application process or the curing process.

- Any two or more components in the agglomerate may be compatible or incompatible with each other. For example,
- 15 the agglomerate may comprise two compatible film-forming components, for example of different colour, or one coloured film-forming component and one uncoloured (compatible) film-forming component (used, for example, to provide additional resin content to improve flow); or
- 20 two incompatible film-forming components, for example of the same colour or one coloured and one uncoloured, and, if desired, a further component which may be compatible with one of the other two components. (For example, the three-component system acrylic, epoxy and polyvinylidene
- 25 difluoride (PVDF) comprises two phases, the PVDF being "compatible" with the acrylic but not the epoxy.)

If desired, one or more of the film-forming

components may contain a non-film-forming additive co-extruded with the film-forming agent. A separate, non-film-forming component may be compatible or incompatible with a film-forming component.

5 As will be explained in more detail below, the presence of incompatible components or components that generate incompatibility (both film-forming and non-film-forming) may be used to produce gloss reduction and/or texture in the powder coating: they are acting as
10 aesthetics additives.

 The incompatibility during film formation can be achieved, for example, by the use of polymers of different chemistry that are immiscible during agglomeration and during curing. For example, an acrylic com-
15 ponent and a polyester, epoxy, polyester-epoxy or polyurethane component are incompatible, and cannot be blended to form a single (stable) phase. Such systems have such different surface tensions that gross defects are caused when one powder "contaminates" the other.

20 Incompatibility during film formation can also be achieved by using components that are initially miscible (compatible) but that become immiscible during curing. Thus, for example, two systems of similar chemistry and approximately the same gel time are compatible, but
25 components with different gel times are initially compatible but become incompatible as curing (and molecular weight build-up) proceeds.

Materials that are incompatible during film-formation can separate into different phase domains which can give rise to incompatibility effects such as matting. Aside from this, the presence of two materials of
5 different surface tension at the surface of the film and in discrete areas/domains can lead to surface disruption (texturing).

Alternatively, incompatible film-forming components, with different surface tensions, may be used to provide
10 multilayer coatings: in this instance they are acting as performance additives.

Aesthetics additives:

Additives having an aesthetic effect include, for example, gloss-reducing additives, texturing agents, and
15 additives to produce lustrous finishes (e.g. metallic and coated mica pigments). Advantageously, these are present as separate components.

A. Gloss-reducing additives:

We have found that a number of additives may be used
20 as separate components in agglomerates of the present invention to reduce gloss.

1. An incompatible film-former; the component may be coloured or uncoloured.
2. A non-film-forming (or non-flowing) polymer, for
25 example PTFE or a cross-linked or high-melting film-former, for example a high melting acrylic such as polymethylmethacrylate (which melts above 200°C);

these are insoluble in the film at the time of film-formation. They may be coloured or uncoloured.

3. Conventional gloss-reducing agents, that is those used for gloss reduction in conventional powder coatings, or extensions of such systems. In general, we believe they act by generating incompatibility in the curing reaction and/or by setting up a differential curing reaction when the coating film is formed. Examples are as follows:

- 10 (a) A second catalyst which will give a much faster gel time than the principal catalyst used to cure the film; examples are the Ciba-Geigy products "XG 125" (zinc N-ethyl-N-phenyl dithiocarbamate) and "XB 3329" (the zinc salt
15 plus a matting wax) that further reduces the gloss level, possibly through incompatibility.
- (b) For pure epoxy and epoxy-polyester (hybrid) systems, a catalyst which has a chemical structure that causes two rates of gelation on
20 curing; examples are given in GB 1,545,780 and include the Hüls products B55 and B68 which are adducts of pyromellitic acid and 2-phenylimidazoline.
- (c) For polyurethane systems using hydroxy-functional polyesters cured with an isocyanate
25 (typically isophorone diisocyanate), a hydroxy-functional polyester with a radically different

functionality (e.g. a hydroxy-functional polyester with a functionality of 7 added to one with a functionality of 2).

- (d) A small proportion of an initially compatible film-former having a different gel time from that of the main film-former; for example for acid functional polyesters designed to cure with triglyceryl isocyanurate, a polyester of approximately the same colour, or uncoloured, but with a different gel time.

4. Inorganic fillers of large particle size, usually up to $30\mu\text{m}$ in size.

We have found that clear "incompatible" particles of mean particle size $< 5\mu\text{m}$ fused in an agglomerate with a conventional powder component or with a film-forming component of smaller particle size, for example of similar particle size to that of the incompatible component, are very effective in producing reduced-gloss systems of very specific and unusual character (very low loss, good flow and levelling, and good flexibility).

Thus, for example, when an acrylic component of small particle size is used as the minor component (up to 20% by weight) with a polyester component 90% by volume of particle size $< 20\mu\text{m}$ in a fused agglomerate, matt coatings caused by micro film defects, with very low gloss levels, may be obtained. Typically, gloss in a polyester system can be reduced to about 5% by addition

of 12% by weight of acrylic component. This second component may be uncoloured or, for example, the same colour as the first component. The system can be further manipulated according to polymer choice, gel time, particle size and filler level of the acrylic. Co-extrusion of such mixtures of materials would give full-gloss films with a degree of stratification of polyester/acrylic through the film. In contrast, using the dry blends of such materials (non-fused) at particle sizes acceptable for electrostatic application gives macro film defects, with some stratification giving rise to a higher than expected (relative to weights added) level of acrylic at the surface. The agglomerated material, however, does not suffer from particle segregation in the solid state as will dry-blended product, thus giving uniformity of product even after transportation and spraying, and the non-spangle matt finishes available using this technique have superior mechanical properties to polyester matt coatings produced by conventional techniques. Such an 'effect' is useful for example on non-reflective ceiling applications.

It should, however, be mentioned that when the acrylic component is added in very small proportions (e.g. 1%) and well mixed, the effects of incompatibility may not be evident. Similarly, with film-forming components of different gel time and of small particle size, the particles are intimately mixed and

incompatibility is at such a small scale that incompatibility effects are not noticeable.

We have also found that PTFE is an effective gloss reducer in fused agglomerates. For example, additions of as little as 10% by weight give films with gloss at 15° (60° gloss). This effect is believed to be highly dependent on the particle size of the additive. However, the cured films mar easily; for example the film can be polished by rubbing with a fingernail, cloth, etc.. We attribute the effect to removal of PTFE at the surface because the additive binds very poorly to the polyester: it is a hard, non-sticky material which does not soften at film-forming temperatures.

Heterogeneous catalysts such as XG 125 and B 55 mentioned above are already used in powder coatings to provide novel effects, for example as matting agents. The catalyst would normally be applied to the milled powder by special techniques, but the agglomeration process of the present invention allows the introduction of a catalyst in a heterogeneous manner.

B. Texturing agents

Conventional texturing agents may be used in agglomerates of the invention, but preferably in a novel way, as separate components in the agglomerate. These include

1. the non-film-forming polymer PTFE,
2. CAB or other suitable film-forming polymer.

By the agglomeration bonding technique of the present invention, the problems encountered in the prior art with the use of texturing agents are avoided.

Thus, agents used as separate components in fused
5 agglomerates may be able to act as matting and/or texturising agents, depending inter alia on the size of the component. Thus, for example, when the size of the PTFE particles in a gloss-reduced composition is increased and the amount of the PTFE component is
10 decreased, a textured finish is produced.

We have found that textured films containing PTFE are less easily marred than gloss-reduced PTFE-containing systems, possibly because there is more free resin to bind each PTFE particle because there is generally less
15 PTFE present, and the texturing PTFE is at a larger size and requires less binding resin.

A modification of the prior art use of high molecular weight thermoplastic added to a thermosetting system is the use of
20 3. a high molecular weight film-forming polymer having a softening point lower than extrusion temperature (90 to 150°C), but higher than agglomeration temperature (preferably 60 to 80°C).

C. Metallic pigments:

Aluminium and a number of other metals and alloys
e.g. stainless steel, copper, tin, bronze and brass (gold
is generally too expensive), may be used to produce what
5 are referred to as 'lustre' or 'glamour' finishes. The
aluminium pigments are the most widely used today.

Leafing systems have already been discussed. Non-leafing
aluminium pigments, which orient themselves throughout
the coating film, provide aesthetics quite unlike leafing
10 aluminium pigments. They are unique in their ability to
project 'flop', polychromatic, and sparkle effects.

('Flop' is the ability to change colour when viewed at
different angles. This capability is directly related to
flake orientation in the film.)

15 Mica pigments may also be used; these are thin
platelets of the natural mineral mica coated with
titanium dioxide and/or iron(III)oxide. The literature
claims that the characteristic properties of their flat
structure, high refractive index and transparency create
20 effects in transparent media which, due to the multiple
reflection of light, match the lustre of pearls or of
mother-of-pearl.

Performance additives:

Various performance additives, the majority of
25 these being non-film-forming components, include a number
that could not be added in conventional powder coating
manufacture. By allowing for the possibility of

incorporating additives post-extrusion, the agglomeration bonding process according to the invention leads in many cases to new products. Examples are:

A. Fragile additives:

5 1. Toughening agents:

Rubber toughening agents are used in the field of composites to prevent crack propagation. In order to be effective they need to have a well-defined size and shape. Extruding or micronising a
10 sample might destroy its morphology and therefore its intrinsic properties, so that in order to maintain the morphology of the rubber toughener it would preferably need to be incorporated by a method other than extrusion. The agglomeration bonding
15 technique of the present invention offers a method of incorporation of rubber tougheners without affecting their morphology. An example is the addition of rubber-like tougheners into acrylic resin systems which are highly durable but mechan-
20 ically weak.

2. Friction-reducing additives:

Low-friction coatings frequently use polytetrafluoroethylene (PTFE) or nylon spheres. Addition of these type of materials by the agglomeration bonding
25 method allows the materials to be used without risk of damage to their morphology, thus leading to the production of low-friction coatings, not producible

by any normal method of powder coating manufacture.

3. Strengthening agents:

Fibres, for example, confer structural strength to composite materials but would not survive
5 extrusion; fibres may also be used to improve conductivity.

4. Microcapsules:

Microcapsules carrying a variety of pay loads can be added to liquid paints to bring about
10 different effects. Many work because application of pressure or stress releases the active ingredient. Those used in the liquid paints that may now be used in the powder coating field, as separate components in a fused agglomerate, include

- 15 - bruisable microcapsules containing perfume,
- bruisable microcapsules containing aggressive solvents, for self-stripping coatings,
- bruisable microcapsules containing ink, dye or chemical precursor of either, for printing and
20 other marking.

There are also some attractive new ideas in this area. For example, the use of

- microcapsules containing air, to improve opacity and perhaps cheapen the coatings,
- 25 - microcapsules carrying plasticizer, to aid flow and levelling (and not necessarily only during stoving, perhaps also after impact of the cured

film, thus providing a self-healing coating);

- microcapsules containing zinc metal, to obtain anticorrosive coatings without the hazards of handling free metal powder;

5 - bruisable microcapsules containing pressure-sensitive adhesives, for example in post-formable coatings stress-induced release of adhesive may improve adhesion at areas of high deformation.

10 B. Materials which may damage or lead to blockage of the extruder:

1. Abrasive materials:

 A non-slip powder coating incorporating sand as the non-slip medium may have a significant market
15 for such things as ladders, gangways, etc..

Other abrasive materials, for example metal carbides, bauxite and certain other solid inorganic material/pigments, may also be used to provide, for example, non-slip coatings, sandpaper or abrasion-resistant coatings. For example, we have found that
20 by including bauxite in a powder formulation, a coating offering substantial abrasive resistance is produced.

As these materials are hard (bauxite extremely so:
25 9 on Mohs scale) such coatings could not be produced by the conventional method due to the excessive wear which would occur to the internals of extruders.

The agglomeration process of the present invention enables this problem to be overcome, leading to the development of a new range of coatings.

In addition, the agglomeration bonding process of
5 the present invention can be used to reduce extruder wear that occurs in conventional powder coatings with the use of certain fillers or extenders such as Syenex extenders. Fillers and/or extenders may be used not only, at large particle size, to reduce gloss (see above), but also as a
10 partial replacement for resin, to reduce costs.

2. Catalysts:

Catalyst: Highly reactive catalysts and/or high levels of catalysts are desired to achieve either fast cure at the most common stoving temperatures
15 (for example 170-220°C) or cure at lower temperatures. However, they would also cause significant cure at extrusion temperatures (usually 90-140°C), that is, the composition would have a short gel time even during extrusion, and this could lead to
20 formation of "bits" in the final coating or even blockage of the extruder. The agglomeration bonding method of powder production according to the invention avoids the need for extrusion of the catalyst and offers a method of incorporating more
25 reactive catalyst and/or higher than normal levels of catalyst.

C. Heat-sensitive materials:

Highly reactive curing agents/catalysts may be used to create ultra-low-bake coatings (baking at little more than extrusion temperature). This allows very heat-sensitive materials, for example

- biological materials (e.g. fungicides or enzymes),
- intumescent pigments and
- thermochromic pigments,

to be included by agglomeration. Intumescent-type pigments foam and yield volatiles when heated and may be used for fire-resistance; such materials in fused agglomerates of the present invention may be included to yield heat- or sound-insulating coatings. Thermochromic pigments are also changed by heat, and are used, for example, on the outside of furnaces to monitor hot spots. Such products may also be used in fused agglomerates of the present invention to provide new and useful coating compositions.

Structuring of products:

In some instances it is desirable to structure the product in a particular way. This can provide advantages in terms of storage and application of the product.

D. Tribocharging and corona-charging additives:

Tribocharging additives are commonly present as free entities in the product, and it is important that they are able to contact the charging surface in the application gun. However, they are known to segregate, causing

problems on application. Introduction of this additive in the last stages of agglomeration may fix them to the surface of the product particle. Corona-charging additives might be used more effectively in a similar way.

5 E. Surface segregation:

Manufacture of the agglomerate in a controlled way also gives us a unique opportunity to control structure in the coating. Our observations suggest that stratification of incompatible phases during film
10 formation is strongly dependent on the initial particle size of the discrete phases.

1. High exterior-durability systems;

Agglomeration of, for example, mixed reduced-size acrylic and polyester powders not only avoids
15 problems of segregation, in the solid state, which is otherwise bound to occur, but also has been found to enhance stratification of the non-compatible phases in the molten state (with respect to 'extruder assembled' particles). This control of
20 film structure offers enormous scope for new and improved products.

Effective multilayer systems containing the best properties of polyester and acrylic polymers have been sought after for some time. Although there is
25 an underlying thermodynamic driving force to separate the two species so that the acrylic lies on the surface of the film, kinetic barriers and the

time constraint of film formation mean that this does not necessarily happen. We believe that use of an agglomerate of the present invention in which the two species start off as reduced-size discrete phases reduces the importance of kinetic barriers.

Other high exterior-durability systems can be devised. Particularly attractive ones use polyvinylidenedifluoride (PVDF). Its use is, however, limited by its poor adhesion to aluminium substrates and it may therefore be co-extruded with acrylic, then reduced in size and assembled in an agglomerate with reduced-sized epoxy, polyester, polyester/epoxy hybrid or polyurethane particles. Stratification of the PVDF/acrylic component over one of these chemistries at the interface provides a one-coat self-priming super-durable system. Alternatively, in some cases PVDF may also be used as film-forming component on its own, for example with epoxy as the other film-forming component; epoxy acts as an adhesion promoter.

2. Silicone non-stick substrates and anti-adhesives:

Silicone-type non-stick substances as used in antifouling coatings technology lack good bulk mechanical properties. Stratification of these film-forming components to yield a thin silicone surface film is advantageous for easy-clean domestic

appliances. Conversely, it may be desirable to achieve stratification of an 'anti-adhesive' to the underside to yield a peelable coating.

F. Porous coatings:

5 Powder coatings lack continuous porosity. It is inferred that because of this any effect which relies on transport through the film is denied. This includes the use of inhibitor pigments for anticorrosion, breathable coatings (e.g. for wood) or many forms of controlled-
10 release. One way to increase porosity may be to increase pigment loading - as a separate component - well beyond critical pigment volume concentration. For example, traditional controlled-release Cu_2O -based antifoulings characteristically have pigment volume concentration
15 >80%. Manufacture of powder coatings having very high PVC is not presently possible, but introduction of porosity may be enabled by the agglomeration process. A possibility is to use a soluble component, for example sodium chloride or other water-soluble inorganic product,
20 at high levels. After formation of the powder coating the water-soluble product may be dissolved away, leaving pores.

We have found that the fusion agglomeration method of the present invention can bring about a dramatic
25 increase in flexibility of the traditional powder manufacturing process and promote utilisation of plant. In our GB Application 2226824 A the concept has been

applied to the production of different colours, but now it is clear that other major parameters can be varied in a similar way. For example, gloss-controlling agents, texture agents and any of the above-mentioned other additives may be introduced at the mixing step for the two coloured components. In essence, formulation is moved further down the production line. The process of the present invention and GB Application 2226824 A also have the advantage of allowing a wide range of products of different appearance (colour, gloss, texture, etc.) to be obtained from a limited number of base colours. The possibility of adjusting pigment or resin content by adding pigment or uncoloured compatible film-forming particles as separate component also assists product flexibility.

Size of agglomerated particles

The size of the fused agglomerate particles is governed by the powder handling characteristics and powder application process and by the desired thickness of the resulting film.

Firstly, size must be consistent with appropriate bulk behaviour. Both particle size and, to a much lesser extent, density influence whether or not a powder is fluidisable, and in general powders having a mean particle size less than $15\mu\text{m}$ are not readily fluidisable, in particular not by commercial electrostatic spray apparatus.

Generally, the agglomerated particles should be fluidisable. A method of measuring the flow properties of a coating powder is that developed at the Verfinstituut TNO (Metal Finishing Journal 1974); the equipment for this method is available as the 'Fluidimeter AS 100'. A standard quantity of powder, 250g, is placed in a vessel similar to a fluidised bed but which is fitted with a 4mm nozzle in the wall just above the porous plate. This nozzle is initially closed and air is passed through the vessel at a standard rate of 200 litres/hour. The powder is stirred during fluidisation until the height of the bed stabilises at a constant level, V_1 , measured in cm. The air supply is switched off, the powder rapidly falls back to the 'at rest' level and the height is again measured, V_0 . The air supply is then switched on again at the same rate as before and the powder allowed to reach a constant height. The nozzle is then opened for 30 seconds and the powder which runs out is collected and weighed in grams; at least five replicate measurements are made and the average (G) calculated. The flow factor, R, is defined by the formula: $R = G \times \frac{V_1}{V_0}$. It has been found empirically that this flow factor correlates very well with practical application properties.

<u>Flow factor, R</u>	<u>Free-flowing properties</u>
> 180	very good
140-180	good
120-140	acceptable
5 80-120	moderate
< 80	poor

Thus, for example, suitable agglomerated powders have flow factor ≥ 80 .

Generally, for a fused agglomerate, particle sizes
10 no more than 1% by volume over $120\mu\text{m}$, for example up to
 $110\mu\text{m}$, preferably up to $100\mu\text{m}$, but preferably at least
90% by volume more than $5\mu\text{m}$, especially at least $10\mu\text{m}$,
should be used. An agglomerate size of up to $150\mu\text{m}$ may
be appropriate for special purposes, for example for
15 powder coating reinforcing bars in concrete. The mean
agglomerate particle size (by volume) generally is no
more than $80\mu\text{m}$, for example no more than $75\mu\text{m}$, preferably
no more than $60\mu\text{m}$, for example no more than $50\mu\text{m}$, or no
more than $40\mu\text{m}$, and generally at least $15\mu\text{m}$, for example
20 at least $20\mu\text{m}$, preferably at least $25\mu\text{m}$. A mean in the
range of from 10 to $50\mu\text{m}$ should especially be mentioned.
Thus, for example, an agglomerate particle size distribu-
tion of 0- $120\mu\text{m}$, preferably 5- $110\mu\text{m}$, more especially 10-
 $100\mu\text{m}$, with a mean particle size (by volume) in the range
25 of from 15- $80\mu\text{m}$, preferably 20- $75\mu\text{m}$, especially 25- $50\mu\text{m}$,
may be used. (It should be noted that the particle sizes
referred to herein are generally measured by light

scattering techniques.)

As to the thickness of the resulting film, for many current applications of powder coating technology, with thermosetting resins the film is approximately 50 μ m thick, but there are many current applications for powder coatings, and a plurality of film thicknesses are used. For decorative finishes, film thicknesses as low as 20 μ m are known, but it is more usual for the film thickness to fall within the range 25-120 μ m, with common ranges being 30-80 μ m for some applications, and 60-120 μ m or, more preferably, 60-100 μ m for other applications, while film thicknesses of 80-150 μ m are less common, but not rare. For functional coatings, similar ranges are found. However, there are some uses (for example, coatings for oil and gas pipe lines and for concrete reinforcing bars) where film thicknesses of 150-500 μ m are common and, for some encapsulation uses, film thickness can be measured in millimetres. In general, however, thinner coatings are cheaper and therefore preferred.

Thus, the size of the agglomerate should generally also be compatible with achieving the minimum suitable film thickness.

Size of component particles

The size of the individual components and the size of the agglomerate are clearly inter-related, and the choice of agglomerate and component particle sizes is influenced by the number and identity of components that

will be in the agglomerate (and their proportions) as well as, in the case of the components, by the desired size of the agglomerate.

In a 50:50 mixture of two particles, for example,
5 for at least 90% by volume of the particles the maximum particle size may be 20-30 μ m, and very often a much smaller size will be appropriate. Once the particle size of one of the components is reduced, the maximum size of another component may be increased.

10 There may also be particular requirements for the size of individual components, so that often the agglomerate will contain components of different sizes.

Colour mixing:

For colour "mixing", that is when two or more
15 differently coloured components are used, a homogeneous colour in the resulting coating is obtained by utilising sufficiently small particle sizes that the difference in colour of individual particles in the resulting coating is not visible to the naked eye. Theoretical
20 considerations put this size at no more than 39 μ m for particles present in a perfect mix. In practice, a perfectly ordered mix is currently unachievable, so the particle size is much less.

This critical size is dependent on a number of
25 factors, including the contrast in hue and luminance between the different particles and the ratio of the different coloured particles. Luminance is somewhat more

important than hue, so that the critical size is lower for a mixture of black and white particles than for a mixture of different coloured particles of similar luminance. For any pair of coloured powders the critical size is lowest for a 1:1 mixture. The critical size is also very dependent on the nature (randomness) of mixing.

For a 1:1 mixture of black and white particles, the critical size for all the particles is about $2.5\mu\text{m}$ for a random mixture. If, however, the mixture is a perfect alternating array of black and white particles, the critical size for all the particles is above $20\mu\text{m}$. The sensitivity of critical size on going to non-perfect mixtures can be accounted for by the statistical probability of the same colour particles lying adjacent to one another.

For random 1:1 mixtures of blue and yellow particles, the critical size is also about $2.5\mu\text{m}$, although this rises to $5.5\mu\text{m}$ for 9:1 mixtures of blue and yellow and to $3.3\mu\text{m}$ for 1:9 mixtures. For random 1:1 mixtures of red and yellow particles the critical size is $3.5\mu\text{m}$, rising to about $5.0\mu\text{m}$ for 9:1 and 1:9 mixtures; mixtures of red and blue particles give similar results. Mixtures of white and yellow particles have a critical size in the range of 10 to $15\mu\text{m}$. Mixtures having three or more coloured components generally have a critical size which is similar to or larger than that of

mixtures of two of the components.

For certain combinations of colour, however, satisfactory mixing to produce a homogeneous colour has proved practicable with 25 μ m particles, especially when
5 dark shades and shades of similar hue (for example, dark bluey-green and dark greeny-blue) are mixed.

Suitably, for colour mixing, at least 90% by volume of the particles of each component have a particle size \leq 25 μ m, for example \leq 22 μ m, advantageously $<$ 20 μ m.
10 Preferably this limit is \leq 15 μ m, advantageously \leq 10 μ m, for example \leq 8 μ m, for example \leq 5 μ m, and usually for example \geq 0.5 μ m, advantageously \geq 2 μ m, preferably \geq 4 μ m, more especially \geq 5 μ m, for example substantially 10 μ m or substantially 5 μ m. 90% by volume of particles in the
15 ranges 0.5-10 μ m, 2-5 μ m, 5-10 μ m, 4-8 μ m and 2-8 μ m should be mentioned. Components in which at least 75% by volume of the particles have such particle sizes should also be mentioned. Generally, no more than 1% by volume should be above 35 μ m and usually all should be below 39 μ m.

20 Thus, for example, for a homogeneous result the particle size of the colour components is advantageously in the range of 0.5 to 15 μ m, preferably 5 to 10 μ m, or 2 to 5 μ m, with the maximum dimension of at least 99% by weight of the particles preferably being in this size
25 range; preferably all the particles have a maximum dimension of 10 μ m or below.

Advantageously the mean particle size for the colour

components for colour mixing is within the range of from 1.5 to 12 μ m, for example 1.5 to 8 μ m. However, mean sizes in the range of from 2 to 8 μ m, for example 2 to 6 μ m, and in the range of from 8 to 12 μ m are especially useful.

5 Mean sizes $\geq 3\mu$ m and $\leq 5\mu$ m should also be mentioned.

It may be convenient to have available standard batches of individual components, for agglomeration for particular uses as and when required. Hence, even where there is no colour mixing, a coloured component used in
10 preparing fused composite particles may have the above particle size.

Speckled finishes:

Alternatively, a speckled finish may be obtained by mixing particles having a size greater than those
15 discussed above. Thus, according to this embodiment of the present invention, the agglomerate comprises components of reduced-sized particles which are nevertheless large enough that when applied to a substrate they are separately visible in the coating; particle sizes $> 20\mu$ m
20 should be mentioned. However, the particle size should be such that the resultant agglomerate of two or more such particles is of a suitable size to meet the requirements for application and film thickness. The desired effect is a film constructed of several individual
25 coloured particle types such that a speckled finish is reproducible and resistant to segregation. At present speckled finishes can only be made by dry-blending normal

particle-sized finished powders and these are susceptible to segregation on transport and application, due to differences in particle size distributions, particle density or chargeability and they therefore give non-reproducible finishes.

Suitably, for a speckled finish, in each component at least 90% by volume of the particles are $<50\mu\text{m}$ and more than 10% by volume of the particles are $\geq 20\mu\text{m}$ and the mean particle size is in the range of from 15 to $35\mu\text{m}$, more especially 20 to $30\mu\text{m}$, for example substantially $25\mu\text{m}$. Preferably, less than 10% by volume are $<10\mu\text{m}$.

"Sooty" powders - colour correction:

The agglomeration bonding technique of the present invention may also be used for colour tinting or correction of the colour of a batch. Thus, if a ready-made coloured powder is found to be failing, a colour specification it may be corrected by the addition of one or more coloured film-forming components or pigment(s).

In the past, colour correction was carried out by adding dry pigments and re-extruding the powder. The re-extrusion and the increased solids:binder ratio may, however, change the film characteristics. By using a coloured film-forming component or pigment component (or single pigment mass tones) and adding either by an agglomeration method according to the present invention, the solids:binder ratio is not dramatically altered and

th additional processing is less severe.

Thus, according to a different embodiment of the present invention, the agglomerate comprises larger-sized (for example, conventionally-sized) coloured film-forming particles and smaller coloured film-forming or pigment particles, for example the reduced-size film-forming particles detailed above for colour mixing, used in amounts preferably of up to 5% by weight, e.g. up to 1% by weight, for example up to 0.5% by weight, more particularly up to 0.3% by weight, to displace the colour of the larger-sized component over a small colour region, this being used for colour tinting or colour correction of a batch. The amount and size of the smaller particles should be such that they are individually not visible in the resulting film. This would allow for correction of colour within a batch without the need for re-extrusion.

Suitably, the larger-sized particles in the agglomerate are more than 10% by volume $\geq 50\mu\text{m}$, and more usually no more than 70% $< 50\mu\text{m}$, with a mean particle size 15 to $75\mu\text{m}$, more usually 25 to $50\mu\text{m}$, preferably 35 to $50\mu\text{m}$, and the smaller-sized particles are at least 90% by volume $< 20\mu\text{m}$, preferably $< 10\mu\text{m}$. Advantageously, all the smaller component particles are $< 25\mu\text{m}$ and no more than 3% are $< 1\mu\text{m}$. Advantageously, the mean particle size of this component is within the range of from 1.5 to $12\mu\text{m}$, for example 2 to $8\mu\text{m}$, preferably 2 to $6\mu\text{m}$ or 8 to $12\mu\text{m}$; mean sizes $\geq 3\mu\text{m}$ and $\leq 5\mu\text{m}$ should especially be

mentioned.

Size of other additives:

An agglomerate of the present invention may also include a special non-film-forming additive(s) as detailed above, and these may be 90% by volume $\leq 30\mu\text{m}$, more especially 20-30 μm , for example substantially 25 μm , in size. Additives with 90% by volume having a size $\leq 25\mu\text{m}$, or 20-25 μm , should especially be mentioned. The size of the additive(s) is dictated, however, not only by the size requirements for the agglomerate (influenced inter alia by the requirements for the resulting film), but also by their specific identity and function. For example, a particle $> 10\mu\text{m}$ in size may produce a visible effect; generally, at least 90% by volume of the component should be below 10 μm to avoid this. Thus, for example, a large-scale texturing effect may be obtained with sand or other inorganic particles at 90% by volume $> 10\mu\text{m}$; when an uncoloured compatible film-forming component is used for adjusting resin content, it is preferably $> 90\%$ by volume $< 20\mu\text{m}$, more especially $> 90\%$ $< 10\mu\text{m}$ as for colour mixing, in order to avoid being separately visible in the resulting coating.

Incompatible film-forming components for matting/
texturing or surface segregation; non-film-forming
components for matting or texturing

As has been mentioned above, an incompatible film-forming component may be used to provide gloss reduction

or texture, or it may be used to obtain a multilayer system.

For a matting effect, discrete domains must be present during film-formation. Thus, as indicated above, 5 components should be incompatible (immiscible) with each other during film-formation; for gloss reduction a difference in surface tension is highly desirable, especially if the domain size is small or if the principal film former is of high molecular weight; for 10 really good results with such systems, and for texturing, a difference in surface tension is probably essential.

With a small domain size, the incompatibility effect achieved generally becomes more pronounced, but with too small a domain size with respect to the wavelength of 15 light, gloss increases.

Film-forming components of similar chemistry but different gel times provide incompatibility during film-formation, but for provision of different surface tensions, a non-film-forming polymer or a film-forming 20 polymer of different chemistry from the principal film-forming polymer, incompatible therewith before curing, is required. An example of the latter is the use of two different thermosetting polymer components such as polyester and acrylic. When the film-forming components 25 have different surface tensions, segregation occurs and enhances matting, so that there is a greater gloss reduction at the same level of addition of second

component, or, for the same effect, the level of addition is less.

The difference in surface tension aids transport of one component to the surface. This component will tend
5 to stratify if the discrete particles start to coalesce, and ultimately a continuous film is produced; whether or not the component coalesces depends on its viscosity and on surface tension: low viscosity and/or low surface tension enhance the tendency to coalesce.

10 For example, an incompatible film-forming component of relatively small particle size may be used to provide a reduced-gloss finish. The nature of the finish varies according to the size of the first film-forming component and the proportions of components. With a polyester
15 component of conventional size and 10% by volume of reduced sized acrylic component, for example, we have obtained a textured matt finish; with the same sizes, but half the amount of acrylic, a "cracked-ice" effect was obtained, and with 10% by volume of reduced-sized
20 acrylic component and a polyester component also of small particle size, a non-textured matt finish was obtained.

Thus, for example, in one embodiment of the present invention the agglomerate comprises a film-forming component of any particle size, but preferably having at
25 least 90% by volume of particles $< 20\mu\text{m}$ and with a preferred mean particle size in the range of from 1.5 to $12\mu\text{m}$, specially 3 to $5\mu\text{m}$ or 8 to $12\mu\text{m}$, and an

incompatible film-forming component having at least 90% by volume of particles $< 20\mu\text{m}$, more especially at least 90% by volume $< 10\mu\text{m}$, and with a preferred mean particle size in the range of from 1.5 to $12\mu\text{m}$, for example 3 to 5 $5\mu\text{m}$ or 8 to $12\mu\text{m}$.

Increases in the quantity of the acrylic component i.e. $> 10\%$ leads to segregation/stratification of the acrylic component at the air interface as evidenced by increasing gloss. The kinetics of this process can be enhanced by using a larger-sized acrylic particle. The degree of stratification occurring depends on the particle size of both the polyester and acrylic particles.

For increased surface separation for multilayer finishes, we believe the particle size in each of the two (incompatible) components needs to be larger, probably approaching the maximum size commensurate with forming a suitable agglomerate.

Suitably, for such multilayer systems, in each component at least 90% by volume of the particles are $< 50\mu\text{m}$ and more than 10% by volume of the particles are $\geq 20\mu\text{m}$ and the mean particle size is in the range of from 15 to $35\mu\text{m}$, more especially 20 to $30\mu\text{m}$, for example substantially $25\mu\text{m}$. Preferably, less than 10% by volume are $< 10\mu\text{m}$.

The additive PTFE, a non-film-forming polymer, has been mentioned as a texturing agent and as a gloss-

reducing additive (and as a friction-reducing additive). Whether a texturing or a matting result is obtained is influenced by the particle size.

For example, if medium-sized or relatively large
5 particles of PTFE are agglomerated with small or relatively small film-forming particles, or medium-sized particles with medium-sized particles, a textured finish is obtained. Thus, for example, in one embodiment, the PTFE has at least 90% by volume of its particles $< 50\mu\text{m}$,
10 more than 10% by volume $\geq 20\mu\text{m}$ and a mean particle size in the range of from 15 to $35\mu\text{m}$, and the film-forming component has at least 90% by volume of particles $< 20\mu\text{m}$, and preferably a mean particle size in the range of from 1.5 to $12\mu\text{m}$, especially 3 to $5\mu\text{m}$ or 8 to $12\mu\text{m}$.

15 However, with smaller particle sizes of the PTFE, the size of the texture is reduced and, when the deformations become sufficiently small, reduced-gloss finishes are obtained.

Similar texturing or gloss-reducing effects at
20 different particle sizes are obtained with CAB, Acronal (Trade Mark) and cross-linked polymers.

Various agglomerate types:

In order to assist in understanding the ramifications and the potential of the fused agglomerates of the
25 present invention, conceptual agglomerates composed of several different combinations of component sizes may be mentioned.

- (I) The agglomerate comprises a larger-sized film-forming component and one or more smaller-sized components, usually a small-sized or relatively small-sized film-forming or non-film-forming component or two or more components of such a size; an example of such a system is the colour correction system described above.
- 5
- (II) The agglomerate comprises two medium-sized components, at least one of which is film-forming, as, for example, in the speckled finish or multilayer system described above; additional small or relatively small-sized components may also be present.
- 10
- (III) The agglomerate comprises two or more small or relatively small-sized components, at least one of which is film-forming, as in the colour mixing system or matt system described above.
- 15
- (IIIA) The agglomerate comprises a large or medium-sized component and one or more smaller-sized components, at least one of the smaller-sized components being film-forming, as, for example, in the textured finish described above.
- 20

More especially, these agglomerate types have particle sizes as follows:

- 25 (I) Component (i): more than 10% by vol. $\geq 50\mu\text{m}$
preferred mean particle size
25-50 μm

- Each component (ii): at least 90% by vol. <20 μ m
preferred mean particle size
1.5-12 μ m
- (II) Each component: at least 90% by vol. <50 μ m
5 more than 10% by vol. \geq 20 μ m
mean particle size 15-35 μ m
- (III) Each component: at least 90% by vol. <20 μ m
preferred mean particle size
1.5-12 μ m
- 10 (IIIA) Component (i): moderate size, e.g.
at least 90% by vol. <50 μ m
more than 10% by vol. \geq 20 μ m
mean particle size 15-35 μ m,
or large-sized
- 15 Each component (ii): at least 90% by volume <20 μ m
preferred mean particle size
1.5-12 μ m

Preferably, components in type III agglomerates and
small-sized components (ii) in types I and IIIA

- 20 agglomerates have particle sizes at least 90% by volume
< 15 μ m, more especially < 10 μ m, often < 2 μ m. Usually all
particles are < 25 μ m and, in a film-forming component, a
maximum, for example, of 3% by volume may be < 1 μ m.

- Preferred mean particle sizes are usually in the range of
25 from 1.5 to 12 μ m, for example 1.5 to 8 μ m, preferably 2 to
8 μ m, for example 2 to 6 μ m, more especially 3 to 5 μ m, or
8 to 12 μ m.

Preferably, components in type II agglomerates and moderate-sized components (i) in type IIIA agglomerates have particle sizes at least 90% by volume substantially $25\mu\text{m}$ and preferably also less than 10% by volume $< 10\mu\text{m}$.

5 Preferred mean particle sizes are in the range of from 20 to $30\mu\text{m}$, more especially substantially $25\mu\text{m}$. Large-sized components in type IIIA agglomerates may be of some considerable size, depending on the effect desired; examples are metallic pigments and sand where the

10 additive cannot be size-reduced without loss of function.

Preferably, large-sized components (i) in type I agglomerates are conventionally-sized powder coating particles. Generally, the components have at least 90% by volume in the range of from 20 to $100\mu\text{m}$ and no more

15 than 70% by volume $< 50\mu\text{m}$, with a mean particle size usually at least $35\mu\text{m}$, for example in the range of from 35 to $60\mu\text{m}$, more often 35 to $55\mu\text{m}$, for example 35 to $50\mu\text{m}$. Alternatively, reduced-sized components may be used, and particle sizes, for example, at least 90% by

20 volume $< 70\mu\text{m}$, for example at least 90% $< 60\mu\text{m}$, or at least 90% $< 50\mu\text{m}$, should be mentioned. Preferred mean particle sizes are in the range of from 25 to $55\mu\text{m}$, more especially, 25 to $50\mu\text{m}$. Thus, for example, the component may be fluidisable alone.

25 Film-forming components in type II agglomerates or in type III agglomerates preferably have the same or similar particle size distributions.

Fillers and other inert particles used to produce gloss reduction or texturing, texturing agents (e.g. PTFE, CAB, Acronal 4F (Trade Mark)), fibres and, especially metallic pigments and mica, and abrasives (especially sand and metal carbides) usually are relatively large particles, and may therefore be incorporated in agglomerates of type II or type IIIA (where they are the larger-sized component).

The particle sizes quoted for the various grades of mica pigments are 5-20 μ m, <15 μ m, 10-50 μ m, 10-60 μ m, 5-100 μ m, 30-100 μ m, 40-200 μ m, 5-50 μ m, 10-100 μ m. From the data available it would appear that the various grades of aluminium pigments have similar particle sizes to the mica pigments.

The size of those additives giving a texture or hammer finish is influenced by their aesthetic function, and may be, for example, 20-30 μ m for CAB used with a metallic pigment to achieve a hammer finish; reduction to a much smaller particle size could adversely affect or even destroy their ability to produce the desired appearance. Other texturing agents are generally conventionally of fine particle size; CAB, Acronal or PTFE, for example, may be used as the smaller component in a type I agglomerate, for example in an amount of < 2% by volume, usually about 1% by volume. At larger particle size CAB and Acronal may be used to achieve novel texturing effects.

It should be noted that for a non-slip surface a smooth film is not required, and, whilst covering by the binder is required, projection of part of the sand or other additive above the surface is not only allowable, but desired (removing one constraint on the component size). Particles of some considerable size (e.g. about 150 μ m) could be agglomerated provided they were a small proportion of the mixture. In such cases the sand will be the larger-sized component in a type IIIA agglomerate. Sand of rather smaller particle size may of course be used for gloss-reduction or texturing.

Pigments, heterogeneous catalysts, rubber tougheners, catalysts, biological material, intumescent and thermochromic pigments, and tribocharging and corona-charging additives are usually required in only small amounts relative to the film-forming component (for example tribocharging additives may be added at 2% or less, usually 1% or less, catalysts also at 2% or less) and/or are effective at small particle size (for example, rubber tougheners are effective at about 1 μ m size).

These are therefore usually present in the agglomerate as relatively small particles, and may therefore be incorporated in agglomerates of types I, III and IIIA (where they are a smaller-sized component).

For rubber tougheners, incorporation in a type III agglomerate should especially be mentioned.

Texturing agents such as PTFE, CAB and Acronal, if

used as very small particles in, for example, type I and III agglomerates, may have a gloss-reducing effect.

Microcapsules, friction-reducing additives, non-film-forming matting polymers and other gloss-reducing agents, fillers and/or extenders used as partial replacement for resin, silicone non-stick substances and anti-adhesives and water-soluble products for introducing porosity may be used in various particle sizes, and may therefore be incorporated in agglomerates of types I, II, III and IIIA. In type II and IIIA agglomerates fillers and/or extenders will also produce a reduction in gloss as mentioned above.

As an alternative to its use in microcapsules, zinc, which unless encapsulated would cause problems because of its conductivity, may be present as the large component in the type IIIA agglomerate; it is thus effectively encapsulated by the smaller film-forming component.

Friction-reducing additives may range in size, for example, from 1 to 30 μ m or more, more especially from 2 to 30 μ m. Excellent results have been obtained with particles 25 μ m in diameter.

Incorporation of silicone non-stick substances and anti-adhesives in a type II agglomerate and of microcapsules in types I and II agglomerates should especially be mentioned.

The size of sodium chloride or other water-soluble component for the preparation of porous coatings should

be chosen carefully, and depends on the size of pores required and on the properties of the coating required, for example water vapour transmission rate, oxygen transmission rate, etc.. Types II and III agglomerates
5 should especially be mentioned.

Reference has already been made to the use of epoxy and PVDF systems. The PVDF may be the inner particle in a type IIIA or type I agglomerate, with a very small amount of epoxy; on film-formation some epoxy migrates
10 to the surface, where it degrades quickly, causing a rapid but minor loss of gloss. The remaining epoxy serves to promote adhesion of the PVDF to the substrate, and also assists the charging and charge retention of the powder and its application to the substrate.

15 The quantity of any performance or aesthetics additive in the agglomerate is dependent on the effect desired and also on the structure of the agglomerate, including the particular sizes of the components.

For example, with a type I agglomerate there may, for
20 example, be on average no more than one layer of small particles per large particle and preferably the large particle should be completely coated. With too large a quantity of additive, the quality of mixing decreases.

Thus, for example, in a type I agglomerate each
25 additive to the larger-sized component may be present in an amount of up to 2% by volume of the total agglomerate. The total amount of such additive(s) may be, for example,

up to 30% by volume.

In a type II agglom rate there may be, for example, at least 20%, preferably at least 30%, by volume of each component, and usually 30 to 50% of additive for a two-
5 component system.

In a type III or IIIA agglomerate there may, for example, be up to 30% by volume of non-film-forming component or components in total.

Speckled agglomerates are possible with a type IIIA
10 agglomerate, as well as with a type II agglomerate, and for these and for colour correction with type I agglomerates and type III agglomerates used for colour mixing, the proportions of film-forming components depend on the desired appearance.

15 Fillers in general should constitute no more than 30% by volume of the agglomerate, preferably no more than 20%, and preferably the filler and pigment together are no more than 30% by volume; usually the filler itself is no more than 5% by volume.

20 Similarly, for example, a coloured or uncoloured incompatible film-forming component used as matting base in any agglomerate type may be up to 30%, preferably up to 20%, more especially up to 15% by volume of the total agglomerate, and more especially at least 5% by volume.

25 With < 5% by volume of incompatible film-forming component a textured finish may be produced. Non-film-forming polymers are suitably up to 20%, preferably up to

10%, for example up to 5% by volume, of total agglomerate. Conventional gloss-reducing additives may be up to 10%, for example up to 5%, by volume of the agglomerate.

5 With increasing amount of acrylic component, the gloss of a polyester, epoxy, polyester-epoxy or polyurethane film increases because the acrylic component tends to coalesce; the extent of gloss increase/coalescence is a function of the concentration of the
10 component and the speed at which it can reach the surface, itself a function of its initial size and of its surface tension versus viscous drag from the surrounding principal film-forming component.

 In a multilayer system, the ratios of segregating
15 components may be, for example, from 90:10 to 50:50, advantageously at least 85:15, preferably 80:20 to 50:50, especially at least 75:25, for example at least 70:30, for example substantially 70:30.

 The present invention especially provides a composition
20 suitable for application as a powder coating and which is in the form of a fused agglomerate of different particulate components comprising a primary film-forming component and a second film-forming or non-film-forming component, the identity, amount and particle size of
25 these components being such that when the powder coating is applied to a substrate and heated to form a continuous coating the components are incompatible and a matting

effect is obtained.

The present invention further provides a composition suitable for application as a powder coating and which is in the form of a fused agglomerate of different particulate components comprising a primary film-forming component and a second film-forming component incompatible with the principal film-forming component, the identity, amount and particle size of these components being such that when the powder coating is applied to a substrate and heated to form a continuous coating the two components segregate and form a multilayer system.

Composition of film-forming systems

A film-forming resin may be a thermosetting resin or a thermoplastic resin. When a thermosetting resin is used, the solid polymeric binder system generally includes a solid curing agent for the thermosetting resin; alternatively two co-reactive film-forming thermosetting resins may be used.

Except where otherwise required for special effect or result, two or more film-forming components (whether coloured or non-coloured) should have similar melting point, melt viscosity, surface tension and other rheological properties, so that they flow and level to the same extent when the powder coating is applied to a substrate, and except where otherwise required for surface segregation any two or more film-forming components are preferably based on the same binder system,

usually of similar composition except for the pigmentation or gel time.

Examples of pigments which may be used in the basic film-forming components or as separate components are

5 inorganic pigments, such as, for example, titanium dioxide white, red and yellow iron oxides, scarlet chrome, chrome yellow and carbon black, and organic pigments such as, for example, phthalocyanine, azo, anthraquinone, thioindigo, isodibenzanthrone,

10 triphendioxane and quinacridone pigments, vat dye pigments and lakes of acid, basic and mordant dyestuffs. Dyes may be used instead of or as well as pigments. Each coloured film-forming component of the coating composition may contain a single colorant (pigment or dye) or

15 may contain more than one colorant.

A pigment content of < 40% by weight of the total pigment and filler content (the filler being added to assist opacity, while keeping costs down) may be used. Usually a pigment content of 25-30% is used, although

20 opacity can be obtained with dark colours with < 10% by weight of pigment.

The powder coating composition may, for example, be based on a solid polymeric binder system comprising a carboxy-functional polyester film-forming resin used with

25 an epoxy-functional curing agent such as, for example, an epoxy resin, for example a condensed glycidyl ether of bisphenol A, or a low molecular weight tri-functional

epoxy compound such as, for example, triglycidyl isocyanurate, or with a beta-hydroxyalkylamide; or a hydroxy-functional polyester used with an isocyanate-functional curing agent; or an epoxy resin used with an amine-
5 functional curing agent such as for example, dicyandimide; or a functional acrylic resin, for example a carboxy-, hydroxy- or epoxy-functional resin, used with an appropriate curing agent. The binder may be a thermoplastic resin such as, for example, a fluoro-resin, for
10 example polyvinylidene fluoride or an ethylene/tetrafluoroethylene copolymer, or poly-phenylene sulphide.

Mixtures of co-extruded film-forming binders may be used; for example a carboxy-functional polyester may be used with a carboxy-functional acrylic resin and a curing
15 agent such as, for example, a beta-hydroxyalkylamide which serves to cure both polymers.

One or more additives such as, for example, a flow-promoting agent, a plasticiser, a stabiliser, for example a stabiliser against UV degradation, or a filler, or two
20 or more such additives may be present in the coating composition, being mixed with a film-forming component(s) before or in the extruder, or present as separate components in the agglomerate. Some additives, however, are unsuitable for co-extruding and must be present as
25 separate components.

Preparation of the agglomerates

The film-forming component(s) and non-film-forming

component(s) where appropriate may be prepared by methods generally known in the production of powder coatings, where appropriate with a final comminution step which produces a low particle size.

5 In general, the film-forming and non-film-forming particles may be of any shape; for example they need not be spherical. Fibres, microcapsules, slip and non-slip additives and metallics, however, are generally of specific shape.

10 The comminution may be carried out, for example, by jet milling in a fluid energy mill. Fluid energy mills function by collision of particles in a high velocity stream of gas, generally air. Particles of diameter less than $5\mu\text{m}$ are easily obtained from a feedstock of mean
15 particle size $50\mu\text{m}$. Fluid energy mills have the advantage that the composition is continuously cooled by the gas stream. In an alternative process the individual component, preferably at particle size below $500\mu\text{m}$, may be dispersed in a non-solvent for the ingredients of the
20 component, for example water, and comminuted by techniques known for wet paint, for example in a high speed bead mill or ball mill. Conventional comminuting devices using metal shearing blades are less efficient in producing sub- $10\mu\text{m}$ particles as it is difficult to
25 prevent fusion of the heat-sensitive powder.

Mixing of the various components may be carried out by various techniques.

A preferred method for mixing film-forming and other particles is dry mixing of the powders in a high-shear mixer. Powders of particle size below $15\mu\text{m}$, for example 0.5 to $10\mu\text{m}$, behave as cohesive non-aeratable powders.

5 Devices containing a high shear chopper, for example, produce satisfactory mixtures of substantially all components of this particle size. High-speed forces may be required to break unwanted agglomerates of particles formed on storage and handling of the components.

10 A simple example of a suitable high-shear mixer is a modification of the type of food mixer known as a liquidiser. An inlet is arranged in the mixing chamber at about the level of the rotating blade. The inlet is for a high-velocity gas stream, preferably air, to ensure
15 that the powder is kept circulating past the blades.

Another example of a suitable high-shear mixer is described in GB Patent 2132128 in which a disintegrator or chopper rotating about the horizontal axis is positioned above a disc rotating about a vertical axis
20 which acts as the main agitator for the mixer. Mixers of this type are sold by Freund Industrial Co. Ltd.

In further examples of suitable high-speed mixers blades of paddles are mounted in a cylinder to rotate about the axis of the cylinder and to scrape the inner
25 surface of the cylinder so that all the powder being mixed is continuously moved around and along the cylinder. The blades may be in the shape of ploughshares

to improve mixing of the powder along the length of the cylinder. Chopper blades are mounted about half way along the cylinder to rotate at right angles to the axis of the cylinder. Such mixers are the Herfeld mixer and
5 that sold by Lodige-Morton Machines Ltd. as the 'Lodige Ploughshare' mixer and by Winkworth Engineering Ltd. under the trade name 'RT Mixer'.

Alternatively, comminuting of film-forming component(s) and other component(s), where appropriate, and
10 mixing may be carried out simultaneously by feeding a mixture of components to a comminuting apparatus such as, for example, a fluid energy mill, or by feeding such a mixture in aqueous dispersion to a bead mill or ball mill. There may be problems in cleaning the comminuting
15 apparatus used in this process, particularly if using wet grinding.

In an alternative mixing process the film-forming and other components where appropriate are mixed by an electrostatic mixing technique. In this process a powder
20 component, for example the colour component, is electrically charged and a second component, for example an uncoloured or second colour component, is not charged or is charged to a different potential, and the powders are mixed. For example, one powder may be electrically
25 charged positively and another powder may be electrically charged negatively. Since the charged particles combine with oppositely charged particles or uncharged particles

preferentially, electrostatic mixing may produce an agglomerated product approaching a perfect mixture rather than a random mixture, thus, where colour is a factor, allowing higher particle sizes to be used than with other forms of mixing; for example, particle sizes of up to 20 μ m for the film-forming powders may be used, even with light and/or dissimilar shades, although particle sizes in the range 1.5 to 10 μ m are preferred. The charged particles may be allowed to combine freely or may be mixed in a pulsed electric feed. A suitable apparatus for electrostatic mixing of powders is described by C.L. Tucker and N.P. Suh in 'Polymer Engineering and Science', October 1976, Vol. 16, at pages 657 to 663.

When three or more powders have to be mixed, for example, two coloured powders and an uncoloured powder or three coloured powders, they are preferably mixed sequentially when electrostatic mixing is used. Alternatively the three or more powders may be charged to different potentials and combined in one mixing operation. For example, if three powders are to be mixed, one may be charged positively, one negatively and the third may be uncharged.

Agglomeration to produce a product with fused composite particles large enough that the material is air-fluidisable and can be applied to the substrate by conventional electrostatic spray, usually 15-100 μ m and preferably 25 to 50 μ m, may be achieved in a number of

ways.

One agglomeration process is granulation in which an added material is used to promote adhesion between the particles.

5 A granulating agent may be added as a solution, but it is important that the solvent does not affect the coating composition. A preferred solvent for the granulating agent is water. The non-volatile constituents in the granulating agent are preferably
10 compatible with the resin in the coating composition. Thus, for an acrylic-based powder coating, a water-borne acrylic granulating agent can be used, such as, for example, Glascol HA2 obtainable from Allied Colloids Ltd. This granulating agent is also suitable for use with
15 thermosetting polyester powder coatings. The granulating agent for an epoxy-based powder coating may, for example, be a water-based epoxy resin. A water-soluble cellulose ether such as, for example, that sold under the Trade Mark "Celacol M20P" is an alternative granulating
20 agent for polyester, acrylic or epoxy resins. The granulating agent may be in the form of a latex, for example a vinyl or acrylic polymer latex. Typically the amount of granulating agent required is less than 15% by weight, for example 1 to 10%, based on non-volatile
25 solids, to agglomerate powder with a mean particle size 5 μ m to yield a product of mean size 40 μ m.

Alternatively, a chemically-harmless solvent for the

binder may be used as granulating agent. The solvent need not be a good solvent for the film-forming components and is preferably quite volatile to aid extraction after agglomeration. An example is methanol (and
5 many other simple alcohols), CFCs, liquid CO₂ and chlorocarbons, especially methylene chloride. Vacuum extraction can be used to aid removal of the solvent after agglomeration.

The granulating agent is preferably introduced as a
10 spray into a mobile mixture. It may for example be so introduced into the apparatus of U.K. Patent 2132128, or into a 'Lodige Ploughshare' or 'Winkworth RT' mixer at a position about half way along the mixing cylinder. When the same machine is used for mixing and agglomerating in
15 this way, dry mixing, if required, should be carried out before addition of the granulating agent. The high-shear chopper is generally not used during granulation, or is used at a much reduced speed. We have found that finely atomised granulating agent allows better control on the
20 product particle size distribution and more efficient use of the granulating agent.

An alternative apparatus which can be used for both mixing and granulating is the 'Spectrum' sold by T.K. Fielder and Co. Ltd. This is of the type having a
25 chopper rotating on a vertical plane above an agitator rotating in a horizontal plane. An aqueous granulating agent may be added after mixing, and the apparatus is

equipped with microwave generators of a frequency to heat the water added with the granulating agent, thus drying to the granulated product.

In an alternative process for introducing the granulating agent, the granulating agent may be encapsulated in particles of the film-forming resin. An aqueous solution of the granulating agent may be emulsified in a solution of the film-forming resin in an organic solvent, for example a solution of a polyether binder resin in a chlorinated hydrocarbon such as, for example, chloroform. The emulsion is spray-dried to form capsules of the desired particle size, for example 1.5 to 10 μ m. These capsules are added to the other component(s) either at the start of mixing or during mixing. The capsules are gradually broken by the shearing forces used in mixing, release the granulating agent solution to cause granulation.

The agglomerated mixture is preferably dried before it is discharged from the mixer to prevent undesired subsequent agglomeration. A drying gas, for example dry air at 25-80°C, may be passed through the mixer after the granulating agent has been thoroughly mixed into the powder coating composition. The mixing action is preferably continued during drying. Alternatively, the agglomerated mixture may be dried in a fluidised bed dryer after discharge from the mixer.

An alternative method of fusion agglomeration is to

use mechanical forces to bind the particles through a process involving deformation and microwelding of the plastic material. A commercially available device for carrying out such mechanical agglomeration is sold as the

5 Nara hybridisation system and described in European Patent Application 224659. Another mechanofusion device is sold by Hosokawa Micron B.V. as an Ang mill. A further apparatus suitable for a mechanofusion agglomeration is a mill having conical and planar dies as

10 described in WO-86/04835. We have shown, for instance, that a material having very broad softening range of 45-80°C may be agglomerated using this device.

A further suitable device is the FM10 Henschel mixer. It relies on a vigorous mixing action to heat up

15 the powder, so that the particles are sufficiently softened to bond under relatively mild impact. The FM10 is a 10 litre chamber featuring a single impeller. The speed of rotation is variable, but typically run at 3000 rpm. A thermocouple is located in the mixer chamber

20 to monitor temperature. Typically, 2 Kg of the mixed components are heated to 50-55°C within 7 minutes. At this temperature bonding occurs. We have found that it is especially advantageous to provide an external heat source to circulate hot water through the external jacket

25 of the vessel.

Thus, in one embodiment of the agglomeration process using a modified Henschel mixer, the vessel is

initially cold and empty, the powders to be mixed are charged to the vessel and stirred at high speed for approximately one minute. The stirrer speed is then reduced to "slow" speed and the hot water passed through the jacket to bring the temperature inside the vessel to 60°C; at this temperature agglomeration proceeds fairly swiftly. This stage of the operation takes approximately 30 minutes. The rate of agglomeration is, we believe, controlled by the rate of heat-up, but the heat-up rate is influenced by the tendency of the powder to stick to the inside wall of the vessel. The provision of a wall scraper is useful to deal with this problem. Once agglomeration has been achieved, the powder may be cooled and sieved.

When there is prior electrostatic mixing of powders before agglomeration, the mixed particles are agglomerated by the attraction of oppositely charged particles. It is however necessary to supplement this with subsequent more permanent agglomeration, for example by a granulation process or by heat softening.

The components may alternatively be mixed and agglomerated by dispersing them together in a liquid dispersion medium followed by drying of the dispersion under conditions causing fusion agglomeration. The liquid dispersion medium is preferably a non-solvent for substantially all the ingredients of the powder coating composition. Water is the preferred dispersion medium.

It may be used alone or with a surfactant or water-miscible organic liquid such as, for example, an alcohol or an ether alcohol.

The mixing apparatus used to form the dispersion may
5 use mechanical means, for example a high-speed mixer which employs a rotating toothed disc to generate high shear forces, or may use ultrasonic dispersion as well as or in addition to the mechanical disperser. For example mixing in a high-speed disperser may be followed by
10 ultrasonic dispersion.

The process used to disperse the composition in the liquid dispersion medium may also serve as the final step in comminuting binder particles of the powder coating composition to the desired particle size, for example to
15 below $10\mu\text{m}$.

The dispersion produced is fed under pressure to the drying apparatus, for example a spray-drying apparatus. Spray-drying may be carried out using a conventional atomising spray head, in which case the diameter of the
20 spray head at its narrowest point is preferably $20\text{--}500\mu\text{m}$ to achieve fused agglomerated particles of the desired particle size for electrostatic spray, namely $20\text{--}50\mu\text{m}$. Spray-drying has the advantage that the particle size of the fused agglomerated powder coating composition
25 produced can be controlled by the concentration of the dispersion and the diameter of the spray head. The spray may alternatively be a centrifugal spray system, for

example a spinning disk spray, or may be an ultrasonic spray. The spray dryer is preferably a co-current dryer in which the direction of the spray is generally downwards and in which a stream of gas, generally air, passes down the drying chamber in the same general direction as the spray. This stream of gas is preferably at ambient temperature or above. The inlet temperature of the gas may, for example, be 40-120°C. The agglomerated powder coating particles produced collect at the bottom of the spray drying chamber and may be removed by a suitable valve system. The vapour of the dispersion medium passes upwards and may be vented. Alternatively the whole output of the spray dryer may be passed to a cyclone separator to isolate the agglomerated powder coating.

When different colours are to be mixed the process of the invention is preferably carried out in conjunction with a data-storage system containing details of the proportions of the colour components required to make powder coating in different shades so that for a given shade and size of batch a data processor can calculate the weight of each colour component to be used. Automatic weighing means may be used if desired. A colour computer may be used if desired to calculate the proportions of colour components required to match a sample of a non-standard shade.

The components may be stored at a reduced particle size, for example below 10 μ m, and mixed and agglomerated

as required. Alternatively the components may be stored at a high particle size, for example 15-50 μ m as conventionally used for coatings, to be comminuted if required, mixed and agglomerated as required.

5 The most common method for the application of powder is an electrostatic spray gun, and the particle size required for most commercial application equipment is ideally a distribution between 10-120 μ m with a mean particle size within the range 15-75 μ m, preferably 25-
10 50 μ m. In the electrostatic spray process the powder coating particles are electrostatically charged by the Corona cloud surrounding the outlet of the spray gun, this cloud being generated by the electrode within the spray gun itself. The charged particles are attracted to
15 the substrate, which is earthed or oppositely charged. Powder coatings may also be applied using tribostatic guns where the powder particles are electrostatically charged by rubbing against the internal winding of the gun. Another method for the application of powder
20 coatings is the use of fluid beds. In this instance the article to be coated is usually preheated and dipped into the fluid bed of powder, the article is then withdrawn and the powder coating allowed to cure by residual heat or by further baking in an appropriate oven.

25 The invention will be further described by way of example with reference to the accompanying diagrammatic drawings of which:

Figure 1 is a diagrammatic section of an apparatus for producing powder coatings by dispersion and spray-drying.

Figure 2 is a diagrammatic section of an apparatus
5 for mixing powdered components by electrostatic mixing.

Figure 3 is a diagrammatic section of an alternative apparatus for mixing powdered components by electrostatic mixing.

Figure 4 is a diagrammatic section of a mixer for
10 mechanically mixing powdered components.

Figure 5 is a diagrammatic longitudinal section of an alternative mixer for mechanically mixing powdered components.

Figure 6 is a diagrammatic cross-section of the
15 mixer of Figure 5 adapted to carry out granulation after mixing.

Figure 7 is a diagrammatic cross-section of an apparatus for mixing and/or granulating film-forming and other components.

20 Figure 8 is a electron microscope photograph of a conventional powder coating composition, and

Figure 9 shows electron microscope photographs of a fused agglomerated powder coating composition.

The apparatus of Figure 1 generally comprises a
25 mixer indicated generally by the reference numeral 10 and a spray dryer indicated generally by the reference numeral 20. The mixer 10 is a high-speed disperser

having an impeller 11 mounted on a shaft 12 within a vessel 13. The vessel 13 has an inlet 15 for the dispersion medium, for example water, and an inlet 16 controlled by a valve 17 for feeding the components. The powder coating particles are dispersed in the dispersion medium and the dispersion thus formed is pumped through an outlet 18 by a pump 19 to a spray dryer 20.

The spray dryer 20 comprises a vessel 21 containing a downwardly directed atomising spray head 22. The spray-dried powder coating particles fall to the bottom of the vessel 21 and are removed through an outlet 24 controlled by a valve 25. The vapour of the dispersion medium which is evaporated passes upwards at the side of the vessel 21 and is vented at 30. Air is fed to the dryer 20 through an inlet 28 and passes in through a heater 29 and down a central duct 33, forming a co-current flow of heated air around the spray head 22.

The apparatus of Figure 2 as shown is suitable for mixing four powders in three mixing steps carried out successively. The apparatus can be adapted to include further mixing steps if required. The apparatus comprises an inlet 41 for a first component whose particles have been positively charged, for example using an apparatus similar to that described in "Polymer Engineering and Science", October 1976, at page 658, and an inlet 42 for a second component whose particles have been negatively charged or are uncharged. The inlet 42

can be sleeved with an insulating material designed to impart a change to the particles by tribocharging. Polytetrafluoroethylene, for example, will induce a negative charge on the particles. The particles mix at the junction 43 of inlets 41 and 42, and the oppositely charged particles combine. The combined particles pass along conduit 46. An inlet 47 for a third component meets conduit 46 at junction 48. The particles of the third powder are preferably oppositely charged to whichever of the first and second powders is present at greater weight, or if the second powder is uncharged the particles of the third composition can be negatively charged. The combined particles and the particles of the third powder combine at junction 48 and pass to conduit 52, where they are combined with particles of a fourth powder component supplied through inlet 53 meeting conduit 52 at junction 54. The fourth powder is charged oppositely to the net charge of the first three powders. The resulting combined particles pass through conduit 55 and can be collected in a suitable container. These may then be granulated to achieve more secure agglomeration.

The apparatus of Figure 3 comprises three inlets 61, 62 and 63 for first, second and third powders. The inlets all feed a mixing chamber 64. The particles of the first powder component are charged positively; the particles of the second powder component are charged negatively and the particles of the third powder

component composition are uncharged. The particles combine in mixing chamber 64 and pass to conduit 65, whence they can be collected in a suitable container.

The apparatus of Figure 4 is a modified 'Moulinex' (Trade Mark) food blender and comprises a mixing chamber 71 containing a blade 72 extending in two directions and mounted on a spindle 73. The blade can be rotated at high speed by drive motor 74. The blade 72 has a sharp leading edge in the direction of rotation and has an upwardly inclined portion 75 at one side of the blade and a downwardly inclined portion 76 at the other side of the blade. The inclined portions 75 and 76 of the blade 72 are both tapered so that the tips of the blade 72 are sharp points. An inlet 77 for high-velocity air is positioned in the wall of the chamber 71 substantially at the level of the blade 72. The chamber 71 has a cover 78 which retains the powder coating particles but is porous to air. The cover 78 can for example be of sintered thermoplastic material such as polypropylene or of sintered glass. The combined action of rotation of the blade 72 and the high-velocity air keeps all the powder in the mixing chamber 71 in a substantially fluid state and the high shear action of the blade 72 breaks up any powder agglomerates, which tend to fall into the path of rotation of blade 72 because of their greater weight than the non-agglomerated powder particles.

The apparatus of Figure 5 comprises a cylindrical

mixing chamber 81 containing blades 82 mounted on a drive shaft 83, which in use is rotated by a motor (not shown). A chopper 84 consisting of a set of cutting blades 85 mounted on spindle 86 is situated half way along the mixing chamber 81. The spindle 86 is driven by a motor 87 to rotate the cutting blades 85. The blades 82 are shaped with a leading edge 88 tapered in two dimensions to a point 89 to promote mixing of powders along the chamber 81. The trailing edge 90 of the blades 82 is also tapered but not to a point.

The apparatus of Figure 6 is a modification of the apparatus of Figure 5 and the same parts have the same numerals. The apparatus includes two types of inlet for a solution of granulating agent. The mixing chamber 81 is modified to include a top zone 91 within which are located a series of spray heads such as 92 fed by pipe 93 so that the spray heads 92 are outside the path of rotation of the blades 82. A further inlet 94 is positioned about half way along the mixing chamber 81 and has its outlet 95 adjacent to the blades 85 of chopper 84.

In use the apparatus of Figure 6 is charged with the required amount of powder and optionally other additives and is operated as a dry mixer initially. When sufficient mixing time has elapsed to obtain a random mixture of particles, a granulation agent is introduced through inlets 93 and 94 and the mixing action is continued to

obtain agglomerated composite particles. After addition of the granulation agent is complete, warm dry air is fed to the mixing chamber 81 through inlets 93 and 94 to dry the powder gradually as it is being agglomerated,

5 limiting the size of the composite particles formed.

The apparatus of Figure 7 is a modified 'Kenwood A516/517' (Trade Mark) food mixer and comprises a motor 101, contained in a housing 102, which drives a stirrer blade 103 within a mixing chamber 104. An air inlet 105
10 leads to an inlet chamber 106, separated from the mixing chamber 104 by a glass sinter 107. High-velocity air can be fed to the inlet 105 to fluidise the powdered material in chamber 104 and warm air can be fed to cause drying during granulation. The product is prevented from
15 escaping during mixing or granulation by a second sintered screen 108 which separates product from exhaust air.

As can be seen from comparison of Figures 8 and 9, (where the size of magnification is shown by each of the
20 white or black scale bars) a fused agglomerate of the present invention is essentially different from a conventional powder. In Figure 8 the powder is > 10% by volume $\geq 50\mu\text{m}$, > 90% by volume < $70\mu\text{m}$, < 70% by volume < $50\mu\text{m}$ and mean particle size 35- $50\mu\text{m}$; Figure 9 shows
25 the result of agglomerating particles 90% by volume < $10\mu\text{m}$ in size.

The following Examples illustrate the invention.

ExamplesHydraulic press method for agglomeration

Agglomeration of particles is achieved by the combination of pressure and temperature.

5 Apparatus:

Moulinex Blender

Moore Hydraulic Press

Steel Press Mould

Moulinex Coffee Grinder

10 Endecotts 106 Micron Laboratory Test Sieve

Procedure:

The appropriate samples are obtained in the desired ratios. Mixing is achieved by two fifteen second runs in a Moulinex blender with scrape-down of the blender's
15 sides between runs. The mixed sample is then transferred to the hydraulic press.

The top and bottom heating plates have a temperature setting of 80°C. The press mould is held between these plates for 45 minutes to allow it to equilibrate from
20 room temperature. Once equilibrated, the bottom half of the mould is lowered to allow the sample to be inserted. Between the sample and the press mould a thin film of non-stick material (PTFE film) is placed to prevent sample adhesion to the mould. The sample is then placed
25 in the centre of the mould and covered with another non-stick film.

The press mould is then closed and the hydraulic

loading is, as swiftly as possible, increased to 20 Tons. This maximum loading is maintained for 30 seconds before being released and the agglomerated sample removed from between the non-stick layers.

- 5 The range in applied pressures is 3×10^6 to $7 \times 10^6 \text{ NM}^{-2}$.

The press mould should be closed and allowed to re-equilibrate for 10 minutes prior to re-use.

- 10 The agglomerated sample has the form of a flat, circular cake. This is micronised by insertion into a Moulinex Coffee Grinder for approximately 20-40 seconds.

- 15 The micronised powder is then sieved through an Endecotts 106 μm laboratory test sieve and collected. The final powder generally has a particle size distribution of 90% < 120 μm and no more than 10% < 10 μm .

Assessment method for electrostatic separation

An assessment technique for the degree of separation in an agglomerated sample and its dry-blended equivalent is listed below.

20 Apparatus:

Volstatic electrostatic gun

Extracted spray booth

Stoving oven (min. 60cm width)

Procedure:

- 25 A 58x10cm steel panel is degreased with xylene and wiped dry. This is suspended horizontally by metal

clips within the extracted spray booth. The Volstatic gun conditions are set at Applied Voltage 60Kv, air pressure 12 lb/in². 40g of sample are inserted into the hopper feed to the gun and the end of the gun barrel
5 positioned exactly 20cm from the centrepoint of the panel. The gun is steadied and activated until all the powder has been applied across one face of the panel without movement of the gun and the panel is placed in the Stoving Oven for the appropriate cure schedule.

10 Assessment:

As the gun is held static during application the film across the panel represents a cross-section of the powder cloud. By studying the variation of specific properties across the panel any segregation of differing
15 particle types is measured. The chosen property to be studied depends on the sample constituents; for example, a matting filler which segregates from the powder would cause a variation in the gloss level across the panel.

A quantitative analysis of the extent of separation
20 is not possible because of differences in film thickness across the panels caused by the static central position of the gun. The film thickness differences may have an underlying influence on the absolute values but can be removed from the overall separation conclusion by
25 comparison of more than one panel.

In the following Examples the following products were used in the film-forming components:

cross-linking agents:

for polyesters: TGIC PT810 (Ciba-Geigy)

5 for acrylics: dodecadonic acid (Hüls)

flow aids/flow aid masterbatches:

Uralac P3188 (carboxy-functional polyester resin containing 10% w/w of Acronal 4F flow aid) (DSM)

Uralac 2518 (DSM)

10 Modarez III (Protex-France)

catalysts/catalyst masterbatches:

Curazole C17Z M/B (carboxy-functional polyester resin containing 10% w/w of Curazole C17Z imidazole-based catalyst) (Inhouse Masterbatch from M & T

15 Chemicals) proprietary catalyst

Zinc stearate A (Durham Chemicals)

waxes:

Worlee ADD1200 (micronised synthetic wax surface property modifier) (Worlee-Chemie GmbH)

20 Carnauba wax (Industrial Waxes)

ACSA Wax (polyethylene wax) (Allied Chemicals)

Benzoin (degassing agent) (SNIA UK)

Blanc fixe (extender) (Manchem Ltd.)

pigments:

25 Bayferrox 3950 (Bayer)

Red Oxide 130BM (Bayer)

Carbon black BP1300 (Cabot/Tennent Group)

Black pearls 1300 bulk use (Cabot/Tennent Group)

Ti-pure R960 (Du Pont)

Tiona RCL472 (SCM Chemicals)

Heucosin Fast Blue G1737 (Heubach Chemicals)

5 TS100 silica (Aerosil) (Degussa)

Xylene (cleaning solvent) (Shell Chemicals)

Example 1

Additions of high levels of catalyst

The catalyst triphenylphosphine (TPP) (supplier
10 M & T Chemicals) supplied in chip form was prepared for
use by coffee grinding using a Moulinex grinder, sieving
to $<106 \mu\text{m}$ and jet milling using a Gueso M100 mill,
micronising air 8 bar, feed air 1.5 bar. The particle
size distribution of the jet-milled catalyst was 99%
15 $< 7.9 \mu\text{m}$, with a mean particle size of $3 \mu\text{m}$.

All formulations produced were based on the white
polyester/TGIC uncatalysed system detailed below:-

	<u>Base Formulation</u>	<u>% by Wt.</u>
	Carboxy-functional polyester (acid value 39-41)	55.31
20	Triglycidylisocyanurate (TGIC)	6.895
	Titanium dioxide pigment	30.00
	Benzoin	0.3
	Flow Aid (Uralac 2518)	7.5
25		<hr/> 100%

The above formulation has a 1:1 stoichiometry.

Three extruded compositions were produced.

- 1) Base formulation (as described).
- 2) Base formulation + 0.2% TPP (by wt. of total composition).
- 5 3) Base formulation + 0.5% TPP (by wt. of total composition).

Manufacture was carried out by extruding each composition using a Buss (RLK46) extruder (set temperature 140°C, screw speed 7), kibbling the extrudate into chip form, grinding the chip using a Moulinex coffee grinder, and finally sieving through a 106 μ m mesh.

Five agglomerated compositions were produced:-

- 4) Base formulation.
- 5) Base formulation + 0.2% TPP (by wt. of total composition)
- 15 6) Base formulation + 0.5% TPP (by wt. of total composition)
- 7) Base formulation + 1.0% TPP (by wt. of total composition)
- 20 8) Base formulation + 2.0% TPP (by wt. of total composition)

For each agglomerated composition 4 to 8, manufacture of the base formulation was carried out by extruding and kibbling as for composition (1) above, and the chip was then milled using a condux mill, and subsequently jet-milled using a Gueso mill (M100) with a micronising air

setting 8 bar and feed air 1-5 bar. The particle size distribution (by weight) of the base formulation was 99% < 16 μm .

Portions of the jet-milled base formulations were dry blend mixed with the indicated portions of jet-milled TPP, and the dry blend mixtures of the powder and catalyst were agglomerated using the hydraulic press agglomeration method described above. The resultant plates of material were ground using a Moulinex coffee grinder and sieved through a 106 μm mesh.

All 8 powder samples were assessed for their gel time at 200°C. The results were as follows:

	<u>% Weight of TPP used</u>	<u>Extruded</u>	<u>Agglomerated</u>
	0	>840 secs	>840 secs
15	0.2	134 secs	157 secs
	0.5	58 secs	94 secs
	1.0	-	66 secs
	2.0	-	37 secs

Those systems with higher than normal levels of catalyst addition (e.g. compositions 7 and 8) showed satisfactory mechanical properties and give the option of faster bake systems. Such levels of catalyst addition were not possible for the extruded compositions.

The extruder used in this experiment was a single screw extruder which was flood fed and temperature was

set at 240°C. Available data shows that the residence time of the material in the extruder ranges from 40 to 125 seconds, with the modal residence time being approximately 55 secs. This data in combination with gel
5 time data illustrates why high level catalyst systems cannot be extruded without significant pre-reaction occurring in the extruder.

Example 2

Low friction coatings

10 The friction-reducing additive, a wax, Du Pont PFA (Trade Mark) (perfluoroalkoxy) powder 532-5010 having a mean particle size: ~30 μm , with 99% <90 μm was used as supplied.

This material was added to the clear powder coating
15 system below:

	<u>% by wt.</u>
Carboxy-functional polyester (acid value 32-36)	51.92
TGIC	6.88
Uralac P3188 (Flow aid masterbatch)	10.00
20 Benzoin	0.3
Carnauba Wax	0.3
Catalyst masterbatch (Curazole C172)	0.6

100% by wt.

25 Four compositions were tested.

1) Clear formulation (normal particle size).

- 2) Dry blend: clear formulati n + 20% (by wt. of total composition) PFA
- 3) Co-extruded: clear formulation + 20% (by wt. of total composition) PFA
- 5 4) Fused agglomerate: clear formulation + 20% (by wt. of total composition) PFA

Composition (1) was manufactured by premixing in a Baker Perkins apparatus for 90 secs; extruding on a Buss (PLK46) extruder (screw speed 12, barrel temp. 140°C
10 (set)); kibbling in a Baker Perkins apparatus; micronising on an ACM3 mill (rotor speed 10900, classifier speed 3600, feed rate 2.5); and finally sieving through a 150 μm mesh. The particle size distribution of the clear formulation after sieving was 99% by weight
15 < 104 μm , with a mean particle size of 32-40 μm .

Composition (2) was prepared by adding the wax to the clear formulation and shaking to mix the components.

In the case of composition (3), the wax was added to the formulation before pre-mixing and co-extruded using
20 the Buss extruder (PLK46) at a set temperature of 140°C and screw speed 8, and the extrudate was micronised by coffee grinding (Moulinex) and sieved through a 106 μm sieve.

In the case of composition (4), the clear component
25 prepared as for composition 1 after sieving was micronised to give a particle distribution of 99% < 10 μm

with a mean particle size of 4 to 6 μ m, and the wax was added to the clear component by solvent agglomeration using 22g of methanol added over 6 mins, and a speed of approximately 300 rpm. During the addition of methanol
5 (BDH Analar), dry compressed air was passed over the sample at approximately 1 litre/min, and after the addition dry compressed air was passed at 15 litres/min for 15 mins. Then the sample was dried for a further 10 mins. before spraying.

10 After drying, the sample was free-flowing and fluidisable, and suitable for electrostatic spraying (only 11% < 10 μ m). The particle size distribution (by weight) was 99% < 87 μ m with a mean particle size 28-37 μ m.

All compositions were applied using standard powder
15 electrostatic spray apparatus (applied voltage 70Kv). The substrate was degreased untreated cold rolled steel (gauge 1mm) panels of approximately 4" x 22". Stoving was for 15 mins at 200°C (total stoving time).

The coefficient of sliding friction was measured
20 using the Ministry of Defence test method DEF STAN 80-73/1 for non-slip deck coatings, using the rubber surface and measuring the coefficient only on the dry surface. The coefficient of friction of composition 4 was found to be half that of composition 1, showing that addition of
25 PFA powder by the agglomeration method described successfully reduced the co-efficient of sliding friction in the

finished film.

Some reduction in coefficient of sliding friction was also obtained with compositions 2 and 3 (i.e. by dry-blend and extrusion methods).

5 Example 3

Incorporation of rubber tougheners

A rubber toughener (Paraloid KH3345 (Trade Mark), ex Rohm & Haas), supplied particle size 98% < 170 μm and mean particle size 90-104 μm was sieved through a 32 μm mesh to give a particle size 94% < 37 μm and mean particle size 21-28 μm .

The rubber toughener was added to a clear polyester/TGIC system with the following formulation:-

	<u>% by wt.</u>
15 Carboxy-functional polyester resin (acid value 35)	91.7
TGIC	6.9
Benzoin	0.4
Flow Agent	1.0
20	<hr/> 100%

Three compositions were manufactured:-

- 1) Clear formulation (as described above).
- 2) Co-extruded composition: clear formulation + 15% (by weight of total composition) rubber toughener.
- 25 3) Fused agglomerate: clear formulation + 15% (by weight of total composition) rubber toughener .

Compositions (1) and (2) were manufactured by extruding on a Buss (PLK46) extruder at temperature 140°C and screw speed 7, kibbling the extrudate into chip form, grinding the chip using a Moulinex coffee grinder, and
5 sieving through a 106 μ m mesh.

In the case of composition (3), the clear component was manufactured by the extrusion, kibbling and grinding steps described above, and then jet milled using a Gueso jet mill M100 with micronising air set at 8 bar and feed
10 air set at 1.5 bar. The rubber toughener was added to the jet-milled powder and this sample was agglomerated by a solvent agglomeration method, 15 g of methanol (Analar ex. BDH) being used with 100g of jet-milled powder/rubber toughener.

15 All three compositions were applied using standard powder electrostatic spray apparatus (applied voltage 70Kv) to a Bonderite 711 Aluminium (1mm) 6"x4" (ex Brent) substrate. All panels were stoved for 15 mins. at 200°C (total stoving time).

20 The Gardener weight impact tester with a falling 1 kg weight was used to assess the impact resistance of all three formulations.

1 joule forward and reverse impacts on all three compositions showed a degree of cracking or crazing. The
25 appearance of the rubber toughened and untoughened panels after impact was markedly different.

With composition (1) (no rubber toughener):

Forward Impact (impact directly onto coating surface):

The failure consisted of a series of continuous concentric circles throughout impact.

5 Reverse Impact (impact onto uncoated side of panel):

The failure consisted of continuous radial lines of failure covering the whole impact area.

With compositions 2 and 3 (15% rubber toughener extruded and agglomerated respectively):

10 Reverse Impact:

Impact resulted in discontinuous cracking with a degree of stress whitening which did not cover the whole impact area.

Forward Impact:

15 Impact resulted in short lines of failure encircling the impact area. Unlike composition (1), these lines of failure did not form continuous concentric circles.

It was demonstrated that addition of rubber
20 toughener caused the nature of the impact failure to change: the rubber toughener reduced the extent of cracking and the lengths of the cracks.

Example 4Gloss reduction by incorporation of an incompatible resin component(a) First example

5	<u>Component A (white, polyester)</u>	<u>% by Wt.</u>
	Carboxy-functional polyester (acid value 29)	45.65
	Uralac P3188 flow aid master batch	7.34
	TGIC	3.42
	Pigment: Ti-Pure R960	15.84
10	Pigment: Tiona RCL472	10.56
	Ac8A Wax	0.20
	Benzoin	0.50
	ADD.1200 Wax	0.50
	Catalyst (zinc stearate A)	0.12
15	Filler (Blanc Fixe)	15.87
	<u>Component B (clear, acrylic)</u>	<u>% by Wt.</u>
	Glycidyl-functional polyacrylate	82.00
	Dodecanedioic acid	16.70
	Benzoin	0.30
20	Flow aid (Modarez III)	1.00

The pre-mixes A and B were each extruded on a Buss PLK46 extruder, screw speed 80 rpm, temperature setting 140°C. The extrudates were then micronised on a Kek mill

and sieved through a 106 μm steel mesh sieve. Both materials were then jet-milled using a Gueso M100 machine operating at the following set conditions: air supply 9 bar, micronising air supply 9 bar, feed air supply 1 bar, material feed rate 70. The particle size distributions obtained were as follows:-

Component A (Polyester)

99% below 25 μm

mean 6 μm

Component B (Acrylic)

99% below 25 μm

mean 3 μm

10 For comparison a powder was also prepared by co-extruding the components A and B in a 85/15 ratio and using otherwise identical procedures.

Components A and B were agglomerated in the ratios 90/10 and 85/15 w/w by the hydraulic press method described above. This produced free-flowing and fluidisable powders with a particle size distribution 90% below 120 μm and means of 30-35 μm , with no more than 10% below 10 μm .

The agglomerated powders were applied by standard electrostatic application techniques using 70 Kv applied voltage and stoved for a total of 15 minutes at 200°C in an electric box oven on a 6'x4'x1 mm chromate pretreated aluminium panel (Ardrox Pyrene - Bonderite 711) substrate.

Assessment of the cured films (of ~50 μ m dry film thickness) for gloss, impact resistance and flexibility on the T bend test gave the following results:-

Gloss (recorded at 20°, 60° and 86°C using a Labor

5 Reflektometer)

	<u>90/10 Agglomerate</u>	<u>85/15 Agglomerate</u>	<u>85/15 Extrudate</u>
20°	4%	2%	31%
60°	10%	6%	77%
86°	16%	8%	93%

10 Mechanicals

	<u>90/10 Agglomerate</u>	<u>85/15 Agglomerate</u>	<u>85/15 Extrudate</u>
Impact R	5 J	2.5 J	2.5 J
Flexibility	1 T	2 T	-

- 15 The figures for impact resistance should be compared with figures for the single component systems which are generally 1 J or less for the acrylic and 10 J or greater for the polyester. The results in the T bend test for flexibility show good results with the 85/15 agglomerate
- 20 and very good results for the 90/10 agglomerate.

A segregation test was carried out on the 85/15 agglomerated composition and on a 85/15 dry blend composi-

tion ('normal' particle size distribution) according to the electrostatic separation method described above.

The 60° gloss showed an even 6% test result across the panel sprayed with agglomerated material, while a spread of 5 between 7 and 30% was obtained for the dry blend material. This demonstrated that no segregation occurred in the agglomerated material, whereas the dry blend separated to some extent on spraying, giving areas rich in either material and therefore gloss variation across the sprayed 10 panel.

(b) Second Example

Component A was a standard white gloss polyester cross-linked with TGIC.

Component B was jet-milled acrylic powder produced as 15 described below.

<u>Composition</u>	<u>Weight (kg)</u>
Methyl methacrylate	1.20
Glycidyl methacrylate	0.50
2-ethyl hexylacrylate	0.30
20 Triganox 21 (peroxide initiator)	0.03
Xylol	2.00

The xylol was heated to reflux and the methacrylate and hexylacrylate materials and 0.025 kg of Triganox initiator were added over a period of two hours while refluxing.

25 Refluxing was continued for a further one hour, and a further 0.005 kg of triganox initiator were then added, and refluxing was continued for another hour. The solvent was distilled off and any remaining was then vacuum stripped

from the product at below 180°C. The product had viscosity 140 Poise (ICI cone and plate) at 200°C, equivalent weight 568, number average molecular weight 9900 and weight average molecular weight 24000.

5 **Acrylic powder manufacture:**

The acrylic powder was incorporated into a simple powder coating formulation according to the proportions shown below.

		<u>% by wt.</u>
10	Acrylic polymer	73
	Dodecanoic acid	15
	Flow aid (Modarez III)	1
	Benzoin	1
	Filler (Blanc fixe)	10

- 15 The above formulation was mixed in a high intensity mixer and extruded on an MPC30 twin screw extruder. (The set temperature was 125°C, screw speed 400 rpm, torque 60%, feed rate 250). The resultant chip was milled (condux mill) and sieved through a 250 micron mesh. This
- 20 powder was further size-reduced using a Gueso M100 jet mill (micronising air 9 bar, feed air 1 bar).

- 25 A Henschel mixer, modified to incorporate a heating jacket, a cooling jacket, scraper blades for the internal wall and inside of the lid, and an air swept bearing for the main rotor, was used for agglomeration.

The agglomeration as carried out as follows: the temperature was set at 72°C, the mixer speed at 2000 rpm for the first minute and then 800 rpm for the remainder of

the process. The machine was charged with 2kg of a 95:5 mix of polyester:acrylic powder. The run time was 30 minutes.

Particle sizes of the starting materials (separately and mixed) and the finished product were determined using a Galai CIS-1 particle sizer. These are presented as evidence of agglomeration.

Size, μm	Polyester Powder	Acrylic Powder	Mixture (95:5)	Finished Product
Mean	56.0	4.7	4.4	62.5
% Vol. $<5\mu\text{m}$	0.56	63.9	3.4	0.75
% Vol. $<10\mu\text{m}$	1.93	99.1	7.9	1.6

A sprayed and cured panel had the following gloss measurements:-

At observation angle	20°	60°	85°
gloss (%) finished product	2%	5	4

The reduction of $< 5\mu\text{m}$ and $< 10\mu\text{m}$ fractions in the Henschel process are good evidence for agglomeration. The excellent matting effect of the acrylic is shown by the gloss measurements. Whereas the finished product sprayed normally during application, the dry mixture behaved as a cohesive powder (clumping, spitting from the gun, uneven

powder cloud density).

Example 5

Production of speckled finishes

An agglomerate was prepared from two coloured poly-
 5 ester/TGIC powders (a blue and a white), the white powder
 having the composition of component A described in Example
 4, and the blue powder being composed as follows:

	<u>% by Wt.</u>
Carboxy-functional polyester (acid value 29)	27.70
10 TGIC	4.50
Carboxy-functional polyester (acid value 30-37)	22.16
Uralac P3188 flow aid masterbatch	11.08
Aca8 Wax	0.30
Benzoin	0.20
15 Pigment: RTC30 (TiO ₂ pigment)	0.82
Pigment: Heucosin Fast Blue G1737	22.16
Filler (Blanc Fixe)	11.08

The pre-mixes for the blue and white powders were each
 separately extruded on a Buss PLK46 extruder at a tempera-
 20 ture setting of 140°C and screw speed 9. The resulting
 extrudates were kibbled and micronised by a Kek mill and
 sieved through 106 µm mesh to give in each case a mean
 particle size of 30-35 µm and distribution of 99% <120 µm
 and no more than 10% <10 µm.

25 The two powders were combined in a ratio of 1:1 by

weight by the hydraulic press method described above. A free-flowing and fluidisable powder of mean particle size of 30-35 μm with distribution of 90% <120 μm and no more than 10% <10 μm was produced.

5 The powder was applied by normal electrostatic spray methods and stoved for 15 minutes at 200°C on aluminium Bonderite 711 panels. The films produced had a uniform heterogeneity in colour, i.e. the degree of speckling was constant across the panel; this was measurable by the
10 Cielab Colour Computer. The flow and levelling and gloss levels remained unchanged as compared with single-coloured panels.

A segregation test was conducted by the electrostatic separation method described above. By colour measurement
15 across the width of the panel any segregation can be witnessed. A dry-blended mixture of the same coloured particles resulted in considerable segregation across the panel, whereas the agglomerated mixture of the same particles showed no significant segregation.

20 Example 6

(a) First example

Colour correction

Three colour components ("colour bases") were prepared using the following pigments

- 1) Bayferrox 3950 Yellow Iron Oxide
- 2) Synthetic Micronised Red Oxide Grade 130BM
- 3) Carbon Black High Colour B.P.1300 Type

1)	<u>Bayferrox 3950 Base</u>	<u>% by wt.</u>
5	Carboxy-functional polyester (acid value 32-36)	66.58
	TGIC	5.73
	Uralac P3188 flow aid masterbatch	10.00
	Carnauba Wax	0.30
	Catalyst Masterbatch (Curazole C17Z)	0.30
10	Bayferrox 3950 pigment	6.48
	Filler (Blanc Fixe)	10.00

Extrusion was carried out in a Buss PLK46 extruder at a temperature setting of 140°C and screw speed 9; micronising was carried out by a Kek mill apparatus. After jet-

15 milling using a Gueso M100 apparatus under a feed air pressure of 0.5 bar, a feed rate of 70 and a micronising air pressure of 8-10 bar, the powder product had a particle size distribution of 99% <8 μm and a mean particle size of 3.4 μm .

20	2) <u>Synthetic Micronised Red Oxide</u>	
	<u>130 BM Base</u>	<u>% by wt.</u>
	Carboxy-functional polyester (acid value 32-36)	71.88
	TGIC	6.13
	Uralac P3188	10.00
25	Carnauba Wax	0.30
	Benzoin	0.30

Catalyst (Curazole C17Z) Masterbatch	0.60
Red Oxide 130BM pigment	5.79
Filler (Blanc Fixe)	5.00

Manufacture was identical to that described for the
5 Bayferrox 3950 base (1) above. The produced powder had a particle size distribution of 99% <8 μm and a mean particle size of 3.9 μm .

3) Carbon Black High Colour

	<u>BP1300 Type Base</u>	<u>% by wt.</u>
10	Carboxy-functional polyester (acid value 32-36)	67.88
	TGIC	5.83
	Uralac P3188	10.00
	Carnauba Wax	0.30
	Benzoin	0.30
15	Catalyst Masterbatch (Curazole C17Z)	0.60
	Carbon Black BP1300 pigment	3.09
	Filler (Blanc Fixe)	12.00

Manufacture was as described in (1) above, except that a screw speed 8 was used in extrusion. The produced powder
20 had a particle size distribution of 99% <8 μm and a mean particle of 3.5 μm .

The colour bases were then added to a conventionally-sized powder coating composition which was slightly off-shade from the desired colour. Calculations using a
25 colour computer gave the amounts of each of the pigments required to achieve colour correction.

Agglomeration was carried out by the hydraulic press method described above. The resultant free-flowing and fluidisable powder had a particle size distribution of 90% < 120 μm and no more than 10% < 10 μm .

- 5 For comparison purposes, the three pigments were used also in a dry pigment addition technique.

The agglomerate was applied by normal electrostatic spray methods and stoved for 15 minutes at 200°C on aluminium Bonderite 711 panels.

- 10 Both correction additive types lead to the colour meeting the specification. The colour bases addition, however, gave a more accurate correction than the dry pigments addition. Close inspection (<15cm) of the dry pigment-corrected film showed a degree of inhomogeneity
15 where areas of varying colours could be just distinguished with the naked eye. This was not seen in the colour base correction. There was no significant variation in flow and levelling caused by increased solids:binder ratio of the films.

20 (b) Second example

Manufacture of components:

A polyester powder of normal particle size distribution was produced by standard methods.

A second polyester component was produced as follows:

	<u>% by wt.</u>
Polyester polymer	76.15
Triglycidyl isocyanurate (TGIC)	5.7
Scarlet chrome sicomin red pigment	16.5
5 Benzoin	0.3
Acrylate flow aid	1.0
Catalyst	0.05

The ingredients were mixed in a high intensity mixer prior to extrusion through a BUSS PR46 Kno-Kneader extruder set
10 at a barrel temperature of 140°C and screw speed of 8.

The chip was ground and sieved to below 250µm before being micronised to 90% by vol. < 10µm particle size in a Gueso M.100 jet-mill (micronising air pressure between 8-10 bar, feed air pressure = 1 bar and powder feed rating = 70).

15 **Agglomeration conditions:**

2kg of a 95:5 by weight mix of normal particle size distribution white polyester : jet-milled orange polyester powder was charged into the modified Henschel apparatus of Example 4b. Conditions in the apparatus were Jacket
20 Temperature Setting of 65-68°C and speed of 1500 rpm for 55 minutes. The mixer speed was adjusted to 1600 rpm and the Temperature Setting increased to 70°C for a further 20 minutes.

Evidence of agglomeration:

25 Panels were sprayed using a stationary electrostatic powder gun aimed at the centre of a panel. The stoved

films should therefore display any separation of the powders due to non-agglomeration by way of the film colour differences at different positions on the panel. Colour computer measurements (ICS Colour Systems Micromatch 9000) were taken on the films at positions that were at the centre of the panel and at a set distance below this (125mm).

The variance in colour between the centre position and the set position in the non-agglomerated starting mixture was compared to the variance in the agglomerated product using the same technique.

		<u>ΔE</u>
15	Starting material	4.69
	Product	0.94

E is a measure of the variance in colour space position between two points and is calculated from:

$$\Delta E = \Delta L + \Delta A + \Delta B$$

where ΔL = variance in luminance axis,
i.e. darker/lighter
where ΔA = variance in green/red axis
where ΔB = variance in blue/yellow axis.

Therefore the lower the value of ΔE the closer the colour is between the positions.

Particle size analyses of the starting materials and the finished product were conducted using a Galai CIS-1 particle analyser.

	Size (μm)	White Polyester	Orange Polyester	95:5 Mix	Agglomerated Product
	Mean	56.0	3.5	52.1	60.6
5	% vol <5	0.6	84.0	2.7	0.4
	% vol <10	1.9	100.0	4.9	1.3

The reduction in <5 μm and <10 μm fractions indicate that such particles have been consumed in agglomeration, and the marginal increase in mean particle size is further evidence of fusion of the large white particles with the much finer tinting powder.

This resulted in a film of a colour that has been tinted away from the colour of the normal particle size base powder.

15 Example 7

Abrasion-resistant coating

Calcined bauxite (300 mesh) FQ0060, an aluminium oxide with up to 12% SiO₂ supplied by C.E. Ramsden, with particle size 99% below 30 μm , mean size 5.8 μm was used as additive.

	<u>Film-forming component</u>	<u>% by Wt.</u>
	Carboxy-functional polyester (acid value 29)	54.67
	Uralac P3188	10.93
	TGIC	4.86
25	ACA8 wax	0.30
	Benzoin	0.20
	Pigment: Black pearls 1300 bulk use	1.70

Filler (Blanc Fixe) 27.34

Addition prior to milling:-

Dry flow additive (silica agent TS100) 0.50

The raw materials for the film-forming component were
5 extruded on a Buss PLK46 laboratory extruder (temperature
set at 140°C, screw speed setting 9) and after addition of
the silica agent micronised in a Kek mill and subsequently
jet-milled using a Gueso M100 machine (feed air pressure 1
bar, micronising pressure 9 bar, feed rate 70) to give a
10 particle size 99% below 20 μm , with mean size 4.5 μm .

Bauxite was added to the powder at 25% by weight and
then processed by the hydraulic press method. The product
was a free-flowing and fluidisable powder, particle size
~ 90% below 120 μm , 10% below 10 μm , mean size 30-35 μm .

15 The agglomerated powder and the film-forming component
were each applied by a standard electrostatic spraying
method (applied voltage 70Kv), to a Taber panel, cold
rolled steel plate 4" square with 1/4" hole centrally
located, 0.04" (1mm) thick. After 15 minutes stoving at
20 200°C, the abrasion resistance of the panels was determined
by the standard test method for Abrasion Resistance of
Organic Coatings by the Taber Abrader as described in ASTM
D4060-84. The following test details were noted:-

Room temperature 20°C

25 Coating thickness approximately 60 μm
Calibrase CS-10 abrasive wheels

1000g applied load

1000 wear cycles

The weight loss for the panel coated in film-forming powder (standard panel) and for the panel coated in agglomerate

5 (test panel) were as follows:

Weight loss for standard panel = 0.050 g

Weight loss for test panel = 0.021 g

This shows that the test panel coated with the agglomerate was more significantly resistant to abrasion than the

10 standard panel.

Example 8

Non-slip powder coating

Sand with a particle size 99% below 180 μm , mean size 120 μm , was dried in an oven, Kek milled and sieved through
15 150 μm mesh, then re-sieved through 106 μm mesh and added in a 1:1 weight ratio to the powdered film-forming component of Example 7.

The components were agglomerated by the hydraulic press method, although the powder was sieved through a
20 150 μm mesh instead of 106 μm mesh as indicated. The product was a free-flowing and fluidisable powder, particle size \sim 99% below 180 μm , 10% below 10 μm , mean size 75 μm .

The agglomerated product and binder were each applied by standard electrostatic spraying method (applied voltage
25 70Kv) to gradient panels, cold rolled steel 565mm x 100mm

x 1mm thick and stoved for 15 minutes at 200°C.

Non-slip properties were measured by a Ministry of Defence Standard test for non-slip deck coatings - DEF STAN 80/73-1 (see Example 2). Tests were carried out on a
5 gradient panel coated with the film-forming component alone (standard panel) and a panel coated with the agglomerated sample. The "non-slip" panel could then be compared with the standard panel to determine the differences in the coefficient of static friction and the coefficient of
10 sliding friction.

An applied load of 5.7Kgs was used in these tests. The same values were obtained for the coefficient of static friction as for the coefficient of sliding friction, as follows:-

15 "Standard" Panel = 0.48
 "Non-Slip" Panel = 0.96

Clearly the "non-slip" panel offers a greater resistance to slip than the "standard" panel.

A segregation test was carried out by the electro-
20 static separation method. Both the "agglomerated" panel and the "dry blended" panel were inspected visually. The sand on the "agglomerated" panel was totally encapsulated by the powder coating and had adhered to the substrate, whereas the sand on the "dry blended" panel had gathered at
25 both ends of the panel and could be brushed off. This showed that segregation had occurred in the "dry blended" panel.

Example 9Addition of Syenex extender

(Syenex is a Trade Mark)

Experimental work has shown that wear rates on
5 extruders processing formulations including very hard
materials such as Syenex extenders are approximately twice
that compared to similar particle size CaCO_3 and BaSO_4
extenders. Their use in the agglomeration process (thus
avoiding extruder wear) was tested as follows:

10 Syenex, supplied by Elkem Nefelin in various grades as
follows:

Syenex 10 - 99% below 8 μm , mean size 2.7 μm

Syenex 20 - 99% below 20 μm , mean size 5 μm

Syenex 30 - 99% below 30 μm , mean size 7.5 μm

15 Syenex 40 - 99% below 44 μm , mean size 10 μm

was added to the powdered film-forming component of Example
7 at 5% by weight and agglomerated by the hydraulic press
method. The product was a free-flowing and fluidisable
powder, having a particle size of 90% below 120 μm , with
20 10% below 10 μm , and a mean size of 30-35 μm .

The agglomerate was applied by the standard electro-
static spraying method (applied voltage 70Kv) to Bonderite
B711 Aluminium panels for normal use and to gradient
panels, cold rolled steel 565mm x 100mm x 1mm thick for the

segregation test. All panels were stoved for 15 minutes at 200°C. Gloss levels were recorded at 20° and 60° using a Labor Reflektometer. Comparison of a panel coated with the standard powder (the binder component alone) with one
5 coated with agglomerated powder showed that Syenex reduced gloss levels, although not very greatly; the coarser the grade of Syenex the more the gloss level was reduced. Comparison of the gloss levels of "extruded" and "agglomerated" panels containing the same grade and amount
10 of Syenex was also made; the "agglomerated" panels produced a slightly larger reduction in gloss level.

The effect of agglomeration on segregation was also tested. The "agglomerated" panel was measured for gloss level using a Labor Reflektometer in five different places
15 and values recorded at 20° and 60°. Measurements were taken at the centre of the test panel, 3" from the centre in both directions and 6" from the centre in both directions. The same procedure was repeated for a dry-blended panel. Results showed the agglomerated panel to have
20 fairly constant readings along its length, whereas the dry blended panel gave widely differing readings along its length, suggesting that separation occurred in the dry blended panel.

Example 10Textured finishes in films by addition of a thermoplastic texturing agent

The texturing agent - cellulose acetate butyrate 551-
5 0.2 (CAB) supplied by Eggar Chemicals as powder, with a
particle size distribution 100% under 188 μm , 5% under
10 μm , and a mean of 96 μm , was used as additive.

The film-forming component had the composition of the
binder component in Example 7, but was prepared by extrud-
10 ing on a Buss PLK46 extruder, at screw speed 80 rpm and set
temperature 140°C, micronising using a Kek mill, sieving
using 106 μm steel mesh hand sieve, and then jet-milled
using a Gueso M100 machine with the following set condi-
tions: feed air pressure 1 bar, micronising air pressure 9
15 bar, feed rate 70. This gave a product with a particle
size 99% below 25 μm and mean 4.5 μm .

This powder was then agglomerated with 0.2% CAB using
the standard hydraulic press method described above to give
a free-flowing and fluidisable powder with a particle size
20 99% below 120 μm , mean 30-35 μm , and no more than 10% below
10 μm . This material was suitable for application by
standard electrostatic application techniques using an
applied voltage of 70 Kv.

Cured films of 50 μm dry film thickness were prepared
25 by spraying onto 6'x4'x1mm chromate pretreated aluminium
panels, Bonderite 711 (Ardrox Pyrene) and stoving for 15

minutes at 200°C total oven time (conventional box oven).

Visual inspection indicates that the agglomerated product gives rise to a textured effect, though this is not as pronounced as for the conventionally prepared material of the same composition. However CAB is not expected to segregate from the agglomerated product on application, whereas it does from conventionally prepared products.

Example 11

Addition of a tribocharging additive

10 **First component:** a polyester gloss powder coating was manufactured using the following formulation:

	<u>% wt.</u>
Polyester polymer	68.1
TGIC	4.6
15 Titanium dioxide	24.9
Other pigments	0.6
Flow agent	1.3
Benzoin	0.3
Wax	0.2

20 A powder of conventional particle size was prepared.

Second component: tribocharging additive jet-milled (77% < 1µm, 99% < 4µm by number). This component was added to the first component in an amount of 1% by weight, based on the weight of the total mixture.

25 The agglomeration of the tribo agent onto the powder particles was achieved using the Henschel equipment

described in Example 4(b). The agglomeration conditions were as follows: temperature at 65°C, mixer speed at 2100 rpm, with 2.4kg of powder containing 1% of tribo additive being added to the mixer. The Henschel apparatus
5 was then run at this speed for 15 minutes, after which time the powder was quickly removed from the vessel and cooled. This sample was now ready for testing on the tribo equipment.

Other reference specimens were also prepared to test
10 how agglomerations of this type performed in terms of its ease of friction charging with respect to identical compositions that had not undergone the same mechanical treatment. These reference samples were as follows:

1) 99% polyester powder plus 1% tribo additive added
15 at the post-milled stage, mixed by simple vigorous shaking together in a plastic bag (thus the tribo additive was a free component).

2) 99% polyester powder plus 1% tribo additive which had been masterbatched in the polyester resin (200°C for 30
20 minutes under nitrogen) prior to the preparation of the sample.

3) 99% polyester powder plus 1% tribo additive which was included in the formulation and added prior to the extrusion stage, though this would not have melted at any
25 point in the processing, unlike the masterbatched material (extrusion takes place at typically 120°C).

4) 100% polyester powder, a control sample.

Testing for tribocharging characteristics was carried out by measuring the charge to mass ratio of each sample on passing through a Nordsen ICAB gun. The powder sample was fed from a fluidised bed through a length of PVC tubing to the inlet of the gun at an approximate rate of 100g/minute. Both the air pressure inside the bed and that passing into the gun was set at a constant 2 bar. Once the powder had been passed through the gun, it was separated from the air stream using a standard cyclone, which also acts to discharge fully the powder, and the build-up of electrostatic charge on the cyclone was measured and used to gauge the tribo-charging that occurred as it passed through the gun. After collection of the powder once it had been separated from the air, its mass over a known period of time was measured and a charge to mass ratio for that particular sample calculated. The sample was then returned to the fluidised bed and another run was taken. Each powder was tested a number of times until the calculated charge to mass ratios were found to stabilise well within the experimental errors of the operation which were around 5%.

The charge to mass data collected on the various powder specimens tested on the tribo equipment is displayed in Figure 10. It can be seen that the pure polyester powder charged significantly less than any of the other samples since the additive itself enhanced the ability of

the polyester to friction charge, irrespective of the way in which it was added to the powder. Moreover, from the quite dramatic reduction in charging from reference sample (1) with run number, loss of the additive must occur
5 during recycling, even when a highly efficient technique of recovery is employed.

Both the masterbatched and extruded samples were found to display enhanced tribo activity, but to a level which under normal circumstances would not be sufficient for
10 satisfactory adhesion of the powder to a metallic substrate. This result appears to support the hypothesis that charge transfer is a surface phenomenon, as the charging of these samples is less than the free additive powder since much of the additive in these cases is trapped inside the
15 particles.

The most significant improvement in the tribo characteristics of any of the samples prepared was, however, found in the agglomerated powder. This powder displayed two important characteristics; firstly, it showed a quite
20 significant increase in its ability to tribo-charge (roughly equal to that of reference sample (1) initially), indicating that the additive was working effectively and, secondly, its magnitude of charging did not appear to diminish with run number as with reference sample (1).
25 This second point is of great significance since it shows that the small additive particles had become physically bonded to the polyester powder and, as a result, loss of

this agent during recycling occurs only at roughly the same rate as loss of the powder itself.

Example 12

Surface segregation (stratification)

5 **First component:** A standard high gloss white polyester was slightly reduced in size by sieving using a 53 μ m sieve to give 90% by volume < 53 μ m.

Second component: A glycidyl-functional acrylic polymer, having equivalent weight 570, viscosity 140 Poise
10 (200°C, ICI Cone and Plate), number average molecular weight 9900 and weight average molecular weight 24000, was granulated to chip size 3-5mm and premixed with other ingredients of the formulation given below before extrusion using a Buss Ko-kneader, with barrel temperature set at 75
15 to 85°C.

	% by wt.
Acrylic polymer	47.5
Dodecanoic acid	11.1
Flow aid (Modarez)	1.0
20 Filler (Blanc fixe)	39.0
Violet pigment	1.0
Benzoin	0.4

The extrudate was cooled and ground, then sieved to 90% by volume < 53 μ m.

25 The polyester and acrylic powders were combined in

80:20 proportions by weight and premixed using a small Moulinex mixer (product I). The composition was agglomerated into a pellet using a Moore's press (hydraulic press method described above) at 100°C for 30
5 seconds. The pellet (product II) was broken into chip, ground and sieved through 106 μ m mesh to yield product III.

For comparison purposes, a mixture of polyester and acrylic powders, identical to that described above, was combined by re-extrusion using a Buss Ko-kneader at 90°C.
10 Powder was obtained from the extrudate as described above (product IV).

Resistance to segregation on application was tested using the standard test described above where powder is sprayed through a stationary gun onto a horizontally
15 positioned panel. Panels were stoved at 180°C for 10 minutes. Colour measurements were made at the centre and 20 cm from the centre of the panel (in a horizontal direction). Since the acrylic powder is violet and the polyester is white, colour measurement gave an indication
20 of the composition on the panel, and colour difference across the panel can be used as a measure of segregation.

In contrast to the agglomerated powder III, the mixture of the polyester and acrylic powder (product I) showed a marked tendency to segregate during application,
25 the polyester preferentially depositing on the centre of the panel and the acrylic tending to deposit away from the

centre.

Colour difference

	ΔE
5 Product I	35.2
Product III	0.6

This clearly demonstrates that agglomeration of the two components prevents segregation during application.

The extent of surface segregation (stratification) was
 10 tested by colour measurements using a Cielab Colour
 Computer (10° observer D65 illuminant). The individual
 components and powders III and IV above were applied to a
 panel and stoved at 180°C for 10 minutes before colour
 measurement. For product II the flat pressed pellet (that
 15 has not been subjected to a stoving treatment) was used;
 this represents the closest approximation to the colour
 generated by mixing the specified proportions of white and
 violet).

	L	a	b
20 White polyester	94.8	-1.1	1.52
Violet acrylic	28.5	13.6	-21.2
Product II	67.4	13.3	-25.6
Product III	54.6	23.9	-35.3
Product IV	65.1	16.0	-28.4

25 III gave a very much deeper shade than IV, and IV deeper

than III.

Comparison of the colour of Product III with that of product II indicates that the acrylic component tended to migrate to the surface during film formation. Comparison
5 of product III with product IV indicates that the migration was much more efficient where the product was manufactured by an agglomeration route, as opposed to co-extrusion of the polyester and acrylic components.

The Example provides confirmation for our view that
10 surface segregation is promoted by having the separating components as discrete domains of substantial size before film-formation begins; in contrast surface segregation is severely retarded when components are intimately blended.

In the above Examples the Buss extruder speed settings
15 correspond to the following actual screw speeds

setting 7 - 75 rpm

8 - 85 rpm

9 - 93 rpm

The feeder for the Gueso M100 jet-mill was an ACCURATGE
20 feeder 310 Model supplied by March Systems Limited.

The above Examples are summarised in the following Table.

TABLE

Example	Size 1st film-forming comp.	Additive	Proportion of additive by wt.	Size of additive	Result	Agglomerate type
1	d	catalyst	0.2 to 2%	d	faster gelling	III
2	d	PtFE-type	20%	99% < 90µm mean 30µm (f)	low friction	IIIA
3	d	rubber toughener	15%	b	improved impact resistance	IIIA
4a	d	uncoloured	10%; 15%	d	gloss reduction	III
4b	c	acrylic	5%			I
5	b	differently coloured polyester	50%	b	speckled finish	II
6a	c	"	as required	d	colour tinting/correction	I
6b			5%			
7	d	bauxite	25%	d	abrasion resistance	III
8	d	sand	50%	> 10% ≥ 50µm	non-slip coating	IIIA
9	d	extender Syenex 10,20 Syenex 30,40	5%	d	cost reduction reduced extruder wear	III
10	d	CAB	0.2%	large - mean 96µm	texture	IIIA
11	c	tribo-charging additive	1%	d	tribo-charging effect retained on recycling	I
12	b	acrylic	20%	b	stratification	II

b = ≥90% by vol. <50µm, >10% by vol. ≥20µm, mean 15-35µm (fluidisable)
 c = >10% by vol. ≥50µm, >90% by vol. <70µm, <70% by vol. <50µm, mean 35-60µm, (fluidisable)
 d = ≥90% by vol. <20µm, mean 1.5-12µm (non-fluidisable)
 (f) = fluidisable (nf) = not fluidisable

CLAIMS

1. A composition suitable for application as a powder coating and which is in the form of a fused agglomerate of different particulate components consisting of a primary film-forming component and one or more other components selected from film-forming and non-film-forming components.

2. A composition suitable for application as a powder coating and which is in the form of a fused agglomerate of different particulate components consisting of a primary film-forming component and one or more other components selected from film-forming and non-film-forming components, provided that,

- if the agglomerate contains a metallic or lustre component and a film-forming component of mean particle size 35 to 60 μ m and no more than 70% by volume < 50 μ m, it also contains an incompatible film-forming component or a non-film-forming performance component or two or more such components, and
- if the agglomerate contains two or more differently coloured compatible film-forming components and optionally an uncoloured compatible film-forming component and the size of the particles in each of those film-forming components is sufficiently low that when the powder coating is applied to a

substrate and heated to form a continuous coating the differences in colour in the cured powder coating arising from the different coloured and any uncoloured particles cannot be discerned by the human eye, it also contains an incompatible film-forming component or a non-film-forming component or two or more such components.

3. A composition suitable for application as a powder coating and which is in the form of a fused agglomerate of different particulate components consisting of a primary film-forming component and one or more other components selected from film-forming and non-film-forming components, provided that,

- if the agglomerate contains a metallic or lustre component and a fluidisable film-forming component, it also contains an incompatible film-forming component or a non-film-forming performance component or two or more such components, and
- if the agglomerate contains two or more differently coloured compatible film-forming components and optionally an uncoloured compatible film-forming component and the size of the particles in each of those film-forming components is sufficiently low that when the powder coating is applied to a substrate and heated to form a continuous coating the differences in colour in the cured powder

coating arising from the different coloured and any uncoloured particles cannot be discerned by the human eye, it also contains an incompatible film-forming component or a non-film-forming component or two or more such components.

4. A composition as claimed in any one of claims 1 to 3, which includes a film-forming component incompatible with the primary film-forming component and/or one or more non-film-forming components.

5. A composition as claimed in claim 1, wherein the different components comprise

- A. a primary, coloured or uncoloured, film-forming component, and
- B. (i) a coloured or uncoloured film-forming component incompatible with the primary film-forming component (A), or
(ii) a non-film-forming performance additive, or two or more of any of such components specified in (i) and (ii)
and/or
(iii) - in the case of a primary film-forming component (A) that is coloured, a further differently coloured compatible film-forming component, the particle sizes of these two

components being such that when the composition is applied to a substrate and heated to form a continuous coating the differences in colour in the cured composition arising from the different coloured particles can be discerned by the human eye, or

- (iv) - in the case of a fluidisable primary film-forming component (A) that is coloured, one or more further differently coloured components selected from colouring pigments and film-forming components compatible with the primary film-forming components, each of such a colour and in an amount and of a particle size sufficiently small that when the composition is applied to a substrate and heated to form a continuous coating the differences in colour in the cured composition arising from the different coloured particles cannot be discerned by the human eye.

6. A composition as claimed in any one of claims 1 to 4, wherein the primary film-forming component is coloured and fluidisable and the agglomerate includes one or more differently coloured components selected from colouring pigments and film-forming components compatible with the primary film-forming agent, each of such a

colour and in an amount and of a size sufficiently small that when the composition is applied to a substrate and heated to form a continuous coating the differences in colour in the cured composition arising from the different coloured particles cannot be discerned by the human eye.

7. A composition as claimed in any one of claims 1 to 4, wherein the primary film-forming component is coloured and the agglomerate includes a differently coloured compatible film-forming component, the particle sizes of these components being such that when the composition is applied to a substrate and heated to form a continuous coating the differences in colour in the cured composition arising from the different coloured particles can be discerned by the human eye.

8. A composition as claimed in any one of claims 1 to 7, which includes two or more coloured compatible film-forming components, the particle sizes of each of these components being sufficiently low that when the composition is applied to a substrate and heated to form a continuous coating the differences in colour in the cured composition arising from the different coloured particles cannot be discerned by the human eye.

9. A composition as claimed in any one of claims 1

to 8, which includes one or more particulate components selected from texturing agents, metallic or mica pigments, colouring pigments and fillers/extenders.

10. A composition as claimed in any one of claims 4 to 9, which includes one or more non-film-forming performance component(s) selected from toughening agents, friction-reducing additives, strengthening agents, microcapsules; zinc; sand, metal carbides, bauxite and other abrasive materials; catalysts; biological material, intumescent pigments, thermochromic pigments, and other heat-sensitive materials; tribocharging additives and corona-charging additives; and water-soluble material.

11. A composition as claimed in any one of claims 1 to 10, which includes a second film-forming component or a non-film-forming component, the identity, amount and particle size of this component and of the principal film-forming component being such that when the powder coating is applied to a substrate and heated to form a continuous coating these components are incompatible and a matting effect is obtained.

12. A composition as claimed in any one of claims 4 to 11, which includes a second film-forming component incompatible with the principal film-forming component,

the identity, amount and particle size of this component and of the principal film-forming component being such that when the powder coating is applied to a substrate and heated to form a continuous coating these two components segregate and form a multilayer system.

13. A composition as claimed in any one of claims 1 to 11, wherein the primary film-forming component is more than 10% by volume $\geq 50\mu\text{m}$.

14. A composition as claimed in any one of claims 1 to 12, wherein the primary and/or another film-forming component has a particle size at least 90% by volume $< 50\mu\text{m}$.

15. A composition as claimed in claim 14, wherein the primary and/or another film-forming component has a particle size at least 90% by volume $< 50\mu\text{m}$, more than 10% by volume $\geq 20\mu\text{m}$ and a mean particle size in the range of from 15 to $35\mu\text{m}$.

16. A composition as claimed in any one of claims 1 to 14, wherein the primary and/or another film-forming component has a particle size at least 90% by volume $< 20\mu\text{m}$.

17. A composition as claimed in claim 16, wherein

the particle size of the primary and/or another film-forming component is at least 90% by volume $< 10\mu\text{m}$.

18. A composition as claimed in claim 16 or claim 17, wherein the mean particle size of the primary and/or another film-forming component is in the range of from 1.5 to $12\mu\text{m}$.

19. A composition as claimed in any one of claims 1 to 6, which comprises

- (i) a film-forming component more than 10% by volume $\geq 50\mu\text{m}$ and mean particle size in the range of from 25 to $50\mu\text{m}$, and
- (ii) a film-forming or non-film-forming component at least 90% by volume $< 20\mu\text{m}$, or two or more such components.

20. A composition as claimed in claim 19, wherein component (i) is no more than 70% $< 50\mu\text{m}$ and has a mean particle size in the range of from 35 to $50\mu\text{m}$.

21. A composition as claimed in claim 19 or claim 20, wherein the or each component (ii), independently of the others, has the size specified in any one of claims 16 to 18.

22. A composition as claimed in any one of claims 1

to 5 or claim 8, wherein each component, independently of the others, is of the size specified in any one of claims 16 to 18.

23. A composition as claimed in any one of claims 19 to 22, wherein the non-film-forming component is selected from colouring pigments, fillers/extenders, non-film-forming polymers, heterogeneous catalysts, toughening agents, friction-reducing additives, microcapsules, catalysts, biological material, intumescent pigments, thermochromic pigments, and other heat-sensitive materials, tribocharging additives, corona-charging additives and water-soluble material.

24. A composition as claimed in any one of claims 16 to 18, which includes as larger-sized component an incompatible film-forming component or a cellulose acetate butyrate resin, a metallic or mica pigment, fibres, zinc, microcapsules, a friction-reducing additive, a non-film-forming polymer, a filler/extender of large particle size, or a water-soluble product.

25. A composition as claimed in any one of claims 1 to 5 or claim 7, wherein each component, independently of the others, has the size specified in claim 15.

26. A composition as claimed in claim 25, wherein

one of the components is a cellulose acetate butyrate resin, a metallic or mica pigment, fibres, zinc, micro-capsules, a friction-reducing additive, a non-film-forming polymer, a filler/extender of large particle size, or a water-soluble product.

27. A composition as claimed in claim 12, which comprises the following incompatible film-forming components:

- (i) acrylic, and
- (ii) polyester,

or

- (i) polyvinylidene difluoride co-extruded with acrylic, and
- (ii) epoxy, polyester, polyurethane or polyester co-extruded with epoxy,

or

- (i) polyvinylidene difluoride, and
- (ii) epoxy,

and wherein the component combinations are as specified in any one of claims 24 to 26.

28. A composition as claimed in claim 27, wherein component (ii) is at least 10% by weight of the total film-forming components.

29. A composition as claimed in claim 27, wherein

component (ii) is from 25 to 50% by weight of the total film-forming components.

30. A composition as claimed in any one of claims 17 to 29, which includes a film-forming component incompatible with the primary film-forming component or a non-film-forming polymeric component for the reduction of gloss.

31. A composition as claimed in claim 30, wherein the gloss-reducing incompatible component has a size as specified in any one of claims 16 to 18.

32. A composition as claimed in claim 30 or claim 31, wherein the gloss-reducing incompatible component is up to 15% of the total film-forming components.

33. A composition as claimed in any one of claims 1 to 32, wherein the mean particle size of the agglomerate is in the range of from 25 to 50 μ m.

34. A composition as claimed in claim 1, substantially as described in any one of the Examples herein.

35. A process for the preparation of a composition as claimed in any one of claims 1 to 34, characterised by providing a primary film-forming component and one or

more other, different, components selected from film-forming components and non-film-forming components, and mixing and agglomerating the components into fused composite particles such that the composition is air fluidisable and can be applied to a substrate by electrostatic spray.

36. A process for the preparation of a composition as claimed in any one of claims 1 to 34, characterised by providing a primary film-forming component and one or more other, different, components selected from film-forming components and non-film-forming components, and comminuting the or at least one of the film-forming components and if appropriate or required one or more non-film-forming component(s), and mixing and agglomerating the components into composite particles such that the composition is air fluidisable and can be applied to a substrate by electrostatic spray.

37. A process as claimed in claim 35 or claim 36, wherein the mixed particles are agglomerated to produce fused composite particles of mean particle size 15 to 80 μ m.

38. A process as claimed in claim 37, wherein the mixed particles are agglomerated to produce fused composite particles of mean particle size 25 to 50 μ m.

39. A process as claimed in any one of claims 35 to 38, wherein the mixing and agglomeration are carried out by a solvent agglomeration process.

40. A process as claimed in any one of claims 35 to 38, wherein the components are mixed as dry powders, and the particles are subjected to mechanical forces sufficient to cause agglomeration of particles by fusion.

41. A process as claimed in claim 35 or claim 36, which is carried out substantially as described herein.

42. A process as claimed in claim 35 or claim 36, which is carried out substantially as described in any one of the Examples herein.

43. A powder coating composition whenever prepared by a process according to any one of claims 35 to 42.

44. Use of an additive selected from film-forming components having a particle size at least 90% by volume $< 50\mu\text{m}$ and more than 10% by volume $\geq 20\mu\text{m}$ and a mean particle size in the range of from 15 to $35\mu\text{m}$; toughening agents, friction-reducing additives, strengthening agents, microcapsules; zinc; sand, metal carbides, bauxite and other abrasive materials; catalysts;

biological material, intumescent pigments, thermochromic pigments, and other heat-sensitive materials; tribo-charging additives and corona-charging additives; and water-soluble material, as a separate particulate component in the preparation of a composition in the form of a fused agglomerate of different particulate components for powder coating a substrate.

45. Use of an acrylic film-former as or in a separate particulate component for addition to a particulate polyester, epoxy, polyester-epoxy or polyurethane component in the preparation of a composition in the form of a fused agglomerate of different particulate components for powder coating a substrate.

46. A process for powder coating a substrate, characterised in that a composition according to any one of claims 1 to 34 or claim 43 is applied to the substrate and heated to form a continuous coating.

47. A substrate coated by a process according to claim 46.

48. A composition as claimed in any one of claims 1 to 34 or claim 43, when used in a powder coating process.

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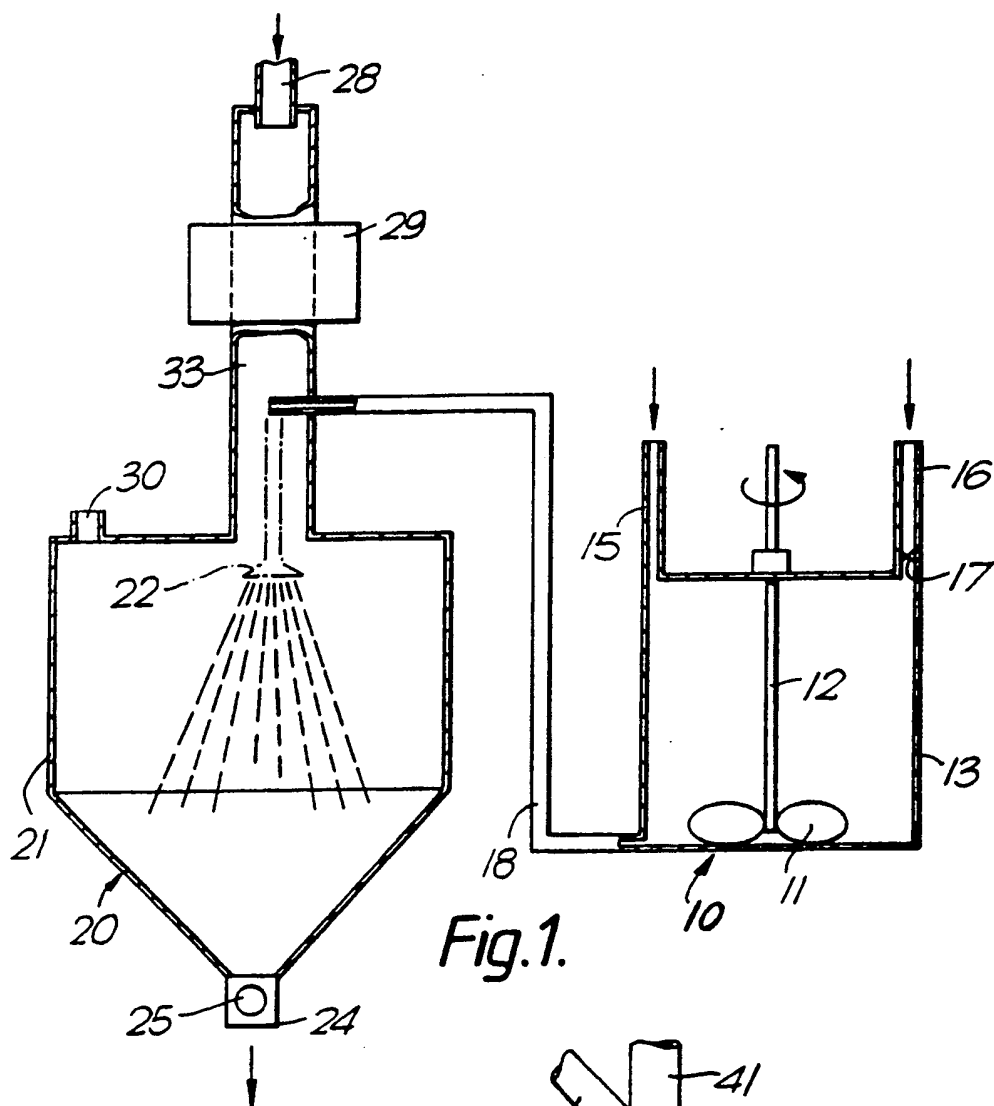


Fig.1.

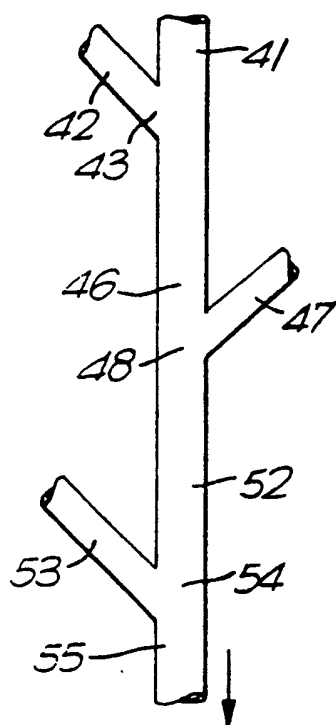


Fig.2.

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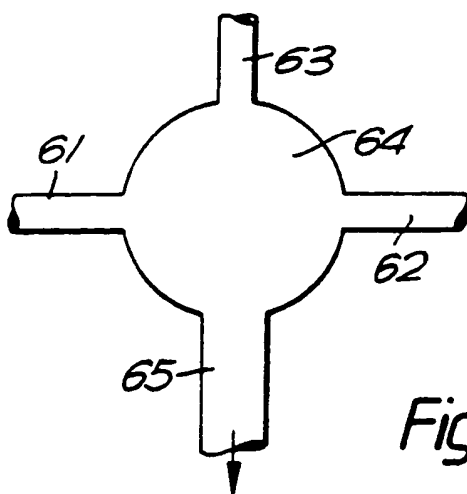


Fig. 3.

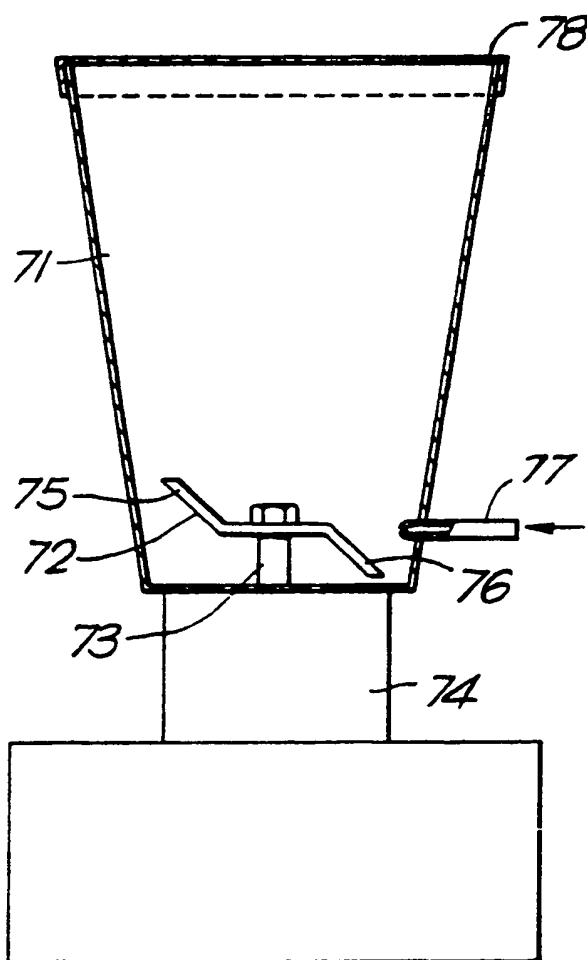


Fig. 4.

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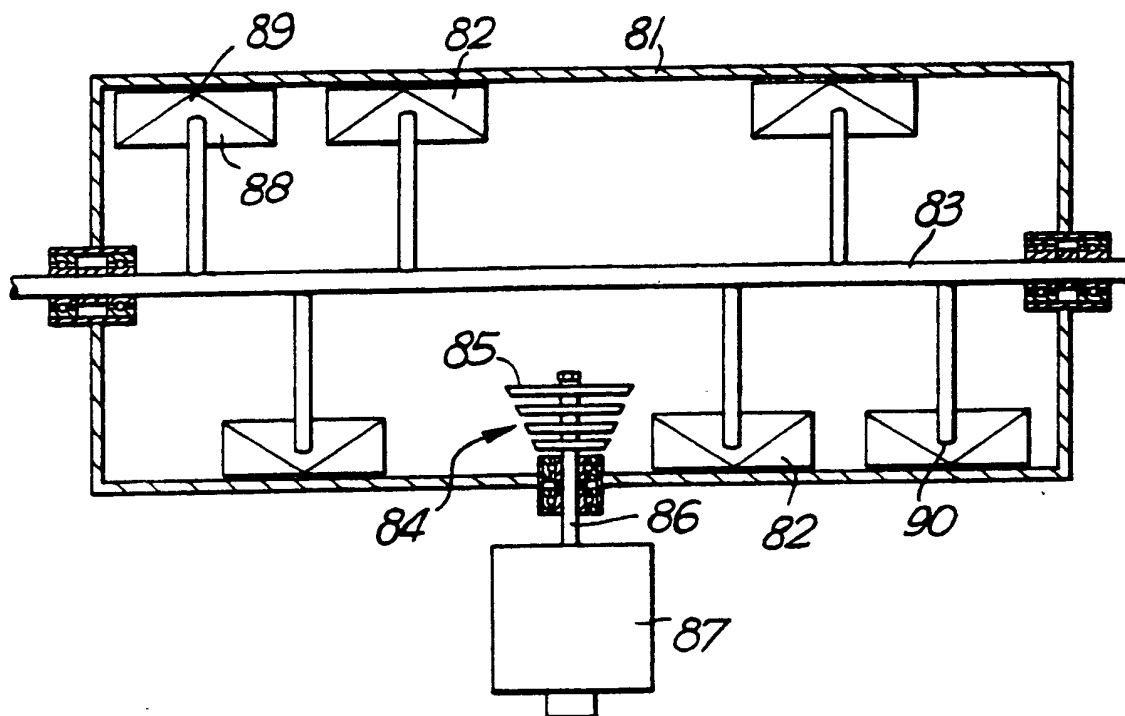


Fig. 5.

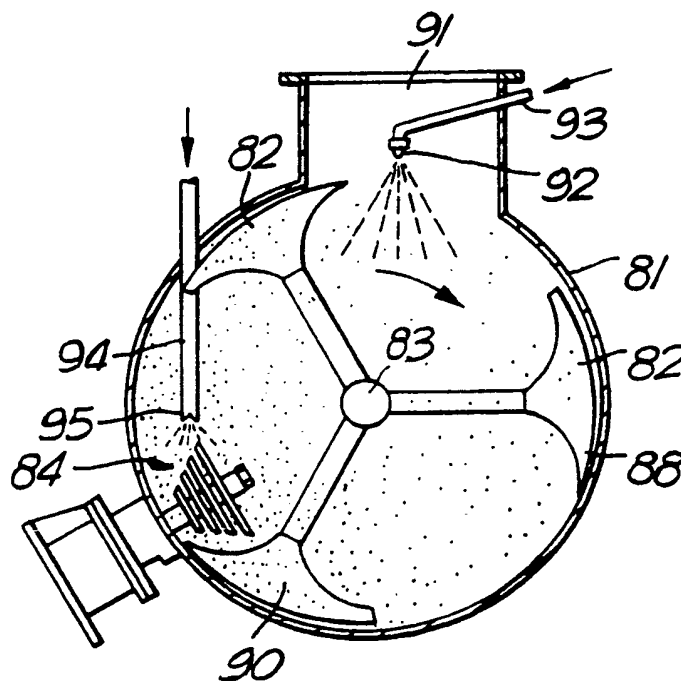


Fig. 6.

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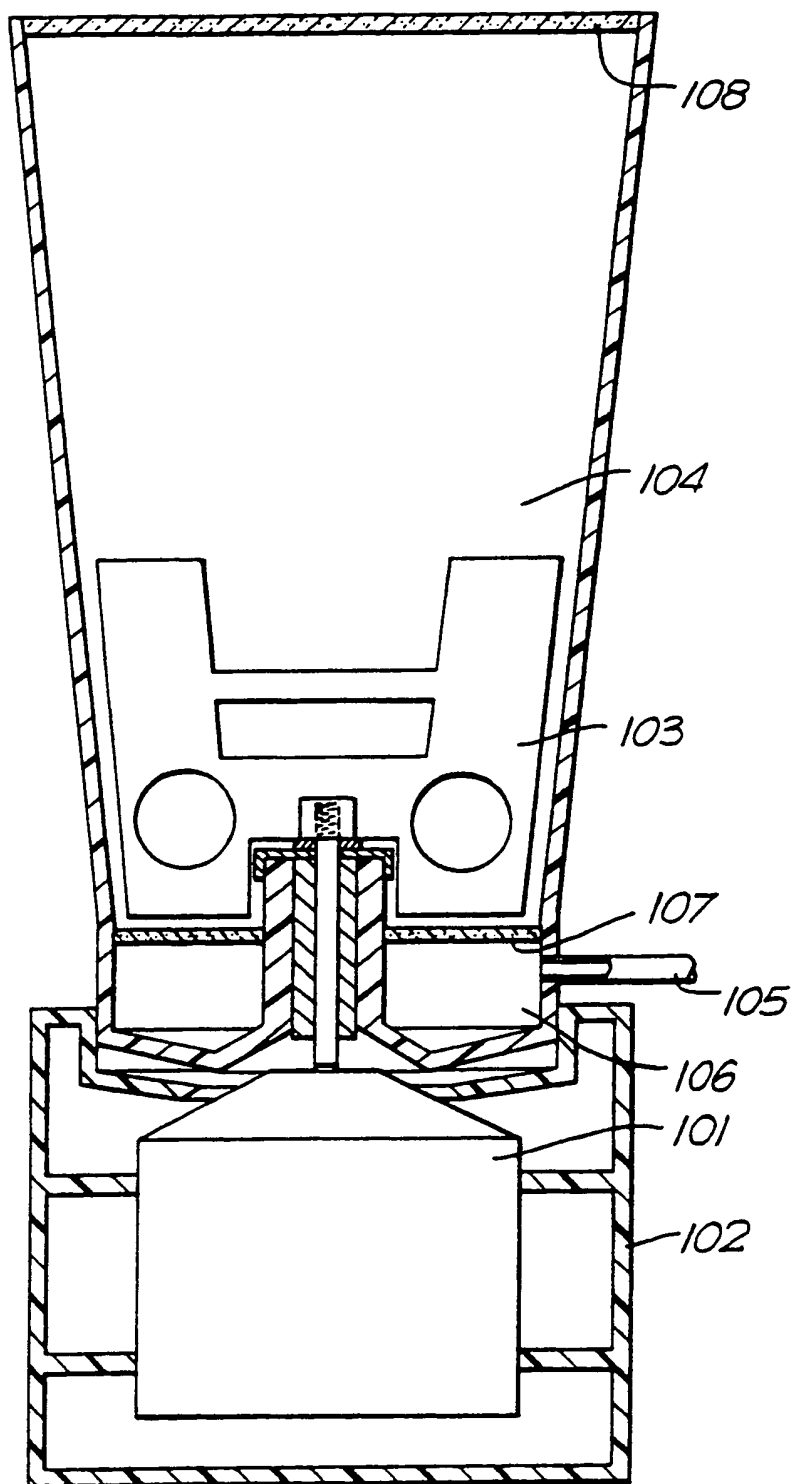


Fig.7.

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Fig. 8.

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*Fig. 9A.**Fig. 9B.*

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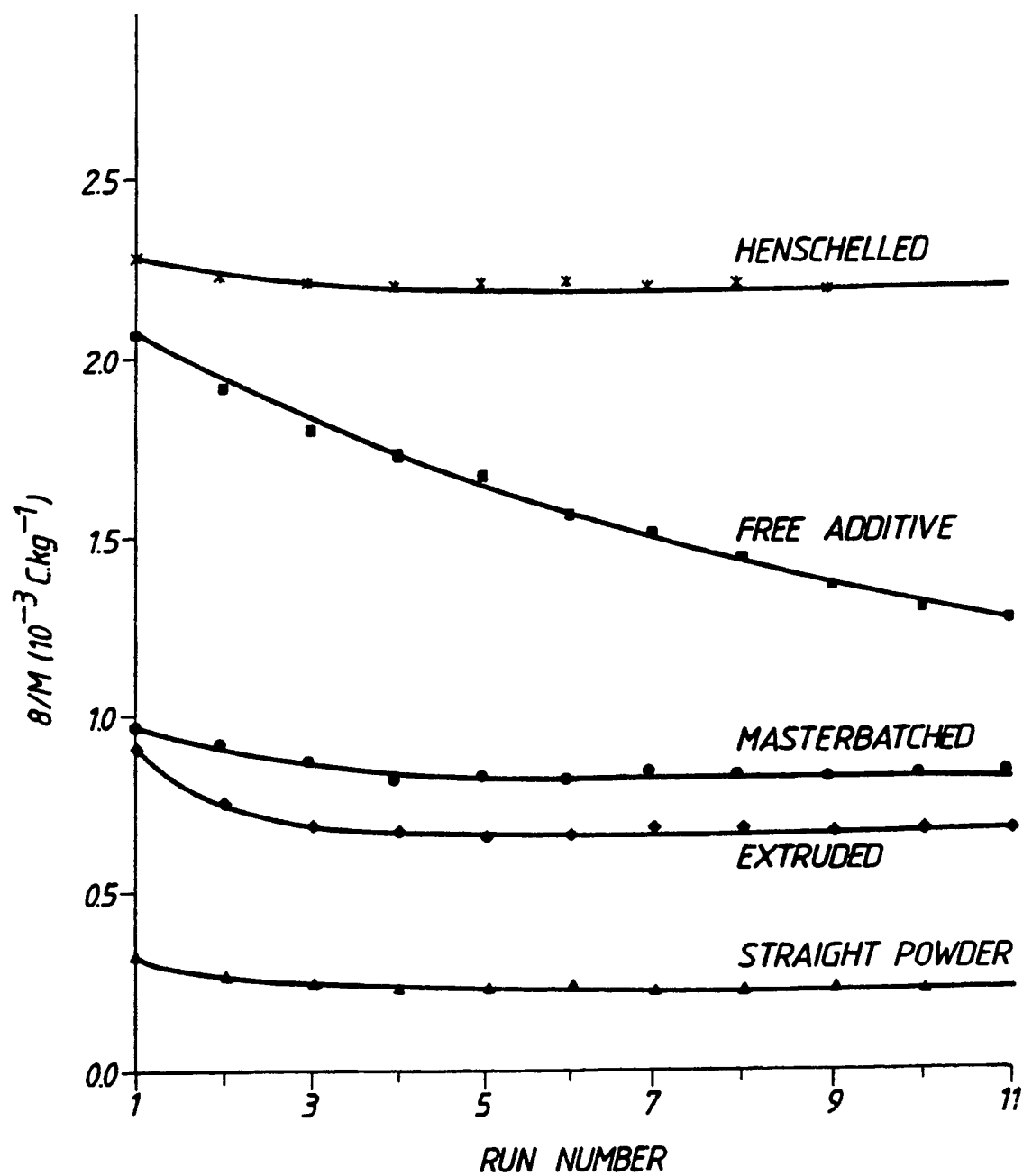


Fig. 10.

SUBSTITUTE SHEET

I. CLASSIFICATION OF SUBJECT MATTER (If several classification symbols apply, indicate all) ⁶ According to International Patent Classification (IPC) or to both National Classification and IPC Int.Cl. 5 C09D5/03 ; C08J3/20														
II. FIELDS SEARCHED <div style="text-align: center; border-top: 1px solid black; border-bottom: 1px solid black; margin: 5px 0;">Minimum Documentation Searched⁷</div> <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 25%; border-bottom: 1px solid black; padding: 5px;">Classification System</td> <td style="border-bottom: 1px solid black; padding: 5px;">Classification Symbols</td> </tr> <tr> <td style="padding: 5px;">Int.Cl. 5</td> <td style="padding: 5px;">C09D ; C08J</td> </tr> </table> <div style="text-align: center; padding: 5px 0;">Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched⁸</div>			Classification System	Classification Symbols	Int.Cl. 5	C09D ; C08J								
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Int.Cl. 5	C09D ; C08J													
III. DOCUMENTS CONSIDERED TO BE RELEVANT⁹ <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 10%; padding: 5px;">Category *</th> <th style="width: 70%; padding: 5px;">Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²</th> <th style="width: 20%; padding: 5px;">Relevant to Claims No. ¹³</th> </tr> </thead> <tbody> <tr> <td style="vertical-align: top; padding: 5px;">P, X</td> <td style="padding: 5px;"> EP, A, 372 860 (COURTAULDS COATINGS) June 13, 1990 see claims; figures 1-7 & GB, A, 2 226 824 (COURTAULDS COATINGS) July 11, 1990 cited in the application <div style="text-align: center;">---</div> </td> <td style="vertical-align: top; padding: 5px;"> 1, 6-8, 35-38, 40-43, 46-48 </td> </tr> <tr> <td style="vertical-align: top; padding: 5px;">A</td> <td style="padding: 5px;"> US, A, 4 260 066 (MARTIN J. HANNON) April 7, 1981 cited in the application see abstract <div style="text-align: center;">---</div> </td> <td style="vertical-align: top; padding: 5px;"> 1, 4, 5 </td> </tr> <tr> <td style="vertical-align: top; padding: 5px;">A</td> <td style="padding: 5px;"> EP, A, 250 183 (NIPPON PAINT CO.) December 23, 1987 cited in the application see claims <div style="text-align: center;">---</div> <div style="text-align: center;">-/-</div> </td> <td style="vertical-align: top; padding: 5px;"> 1, 9 </td> </tr> </tbody> </table> <div style="font-size: small; padding: 5px 0;"> ⁹ Special categories of cited documents : ¹⁰ <div style="display: flex; justify-content: space-between;"> <div style="width: 48%;"> <p>^{"A"} document defining the general state of the art which is not considered to be of particular relevance</p> <p>^{"E"} earlier document but published on or after the international filing date</p> <p>^{"L"} document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>^{"O"} document referring to an oral disclosure, use, exhibition or other means</p> <p>^{"P"} document published prior to the international filing date but later than the priority date claimed</p> </div> <div style="width: 48%;"> <p>^{"T"} later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>^{"X"} document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>^{"Y"} document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>^{"A"} document member of the same patent family</p> </div> </div> </div>			Category *	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claims No. ¹³	P, X	EP, A, 372 860 (COURTAULDS COATINGS) June 13, 1990 see claims; figures 1-7 & GB, A, 2 226 824 (COURTAULDS COATINGS) July 11, 1990 cited in the application <div style="text-align: center;">---</div>	1, 6-8, 35-38, 40-43, 46-48	A	US, A, 4 260 066 (MARTIN J. HANNON) April 7, 1981 cited in the application see abstract <div style="text-align: center;">---</div>	1, 4, 5	A	EP, A, 250 183 (NIPPON PAINT CO.) December 23, 1987 cited in the application see claims <div style="text-align: center;">---</div> <div style="text-align: center;">-/-</div>	1, 9
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IV. CERTIFICATION <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; border-bottom: 1px solid black; padding: 5px;"> Date of the Actual Completion of the International Search <div style="text-align: center;">18. OCTOBER 1991</div> </td> <td style="width: 50%; border-bottom: 1px solid black; padding: 5px;"> Date of Mailing of this International Search Report <div style="text-align: center;">05. 11. 91</div> </td> </tr> <tr> <td style="border-bottom: 1px solid black; padding: 5px;"> International Searching Authority <div style="text-align: center;">EUROPEAN PATENT OFFICE</div> </td> <td style="border-bottom: 1px solid black; padding: 5px;"> Signature of Authorized Officer <div style="text-align: center;">GIRARD Y.A. </div> </td> </tr> </table>			Date of the Actual Completion of the International Search <div style="text-align: center;">18. OCTOBER 1991</div>	Date of Mailing of this International Search Report <div style="text-align: center;">05. 11. 91</div>	International Searching Authority <div style="text-align: center;">EUROPEAN PATENT OFFICE</div>	Signature of Authorized Officer <div style="text-align: center;">GIRARD Y.A. </div>								
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III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)		
Category *	Citation of Document, with indication, where appropriate, of the relevant passages	Relevant to Claims No.
A	DE,A,2 147 653 (STRUMHAUS JAROSLAV) April 5, 1973 see claims ---	1,4,5
A	FR,A,2 310 394 (UNILEVER) December 3, 1976 see claims ---	1
A	US,A,3 980 607 (GERHARD JOHANNES) September 14, 1976 see abstract ---	1,9
A	FR,A,2 190 874 (TOYO BOSEKI K.K.) February 1, 1974 see page 3, line 17 - line 22 see page 7; example 5 see claims 1,2 ---	1,27-29, 45

ANNEX TO THE INTERNATIONAL SEARCH REPORT ON INTERNATIONAL PATENT APPLICATION NO.

GB 9100868
SA 48159

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

18/10/91

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EPO FORM P0679

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82

16. A powder coating composition as claimed in claim 15, wherein the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2a) is in the range of from 1:99 to 40:60 by weight.

5 17. A powder coating composition as claimed in claim 16, wherein the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2a) is in the range of from 1:99 to 30:70 by weight.

10 18. A powder coating composition as claimed in any one of claims 1 to 17, wherein the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2a) is in the range of from 5:95 to 30:70.

15 19. A powder coating composition as claimed in any one of claims 1 to 18, wherein the uncoloured film-forming component or components (2) are present in an amount of at least 50% by weight of the total film-forming components.

20 20. A powder coating composition as claimed in claim 19, wherein the uncoloured film-forming component or components (2) are present in an amount of at least 60% by weight of the total film-forming components.

21. A powder coating composition as claimed in claim 20, wherein the uncoloured film-forming component or components (2) are present in an amount of at least 70% by weight of the total film-forming components.

25 22. A powder coating composition as claimed in any one of claims 2 to 21, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 20% by weight of the total film-forming components.

23. A powder coating composition as claimed in claim 22, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 30% by weight of the total film-forming components.

5

24. A powder coating composition as claimed in claim 23, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 40% by weight of the total film-forming components.

10

25. A powder coating composition as claimed in claim 24, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 50% by weight of the total film-forming components.

15

26. A powder coating composition as claimed in claim 25, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 60% by weight of the total film-forming components.

20

27. A powder coating composition as claimed in any one of claims 1 to 26, wherein there is no more than 15% by weight, calculated on the weight of total film-forming components, of uncoloured film-forming component(s) (2b).

28. A powder coating composition as claimed in any one of claims 1 to 24, wherein there are two or more compatible coloured film-forming base components (1).

25

29. A powder coating composition as claimed in any one of claims 1 to 28, wherein the uncoloured film-forming component (2a) or at least one of the uncoloured

PATENT COOPERATION TREATY

From the
INTERNATIONAL PRELIMINARY EXAMINING AUTHORITY

To:

SENIOR, Janet et al.
ABEL & IMRAY
20 Red Lion Street
London WC1R 4PQ
GRANDE BRETAGNE

ABEL & IMRAY			
CASE NO. 4750			
G.O. WA MA			
14 JUN 2001			
A/C?	Y	N	<input checked="" type="checkbox"/>
CPA?	Y	N	COPIED

PCT

NOTIFICATION OF TRANSMITTAL OF
THE INTERNATIONAL PRELIMINARY
EXAMINATION REPORT

(PCT Rule 71.1)

Date of mailing
(day/month/year) 12.06.2001

Applicant's or agent's file reference
4750/Deb 3

IMPORTANT NOTIFICATION

International application No.
PCT/GB00/00871

International filing date (day/month/year)
09/03/2000

Priority date (day/month/year)
10/03/1999

Applicant
INTERNATIONAL COATINGS LIMITED et al.

1. The applicant is hereby notified that this International Preliminary Examining Authority transmits herewith the international preliminary examination report and its annexes, if any, established on the international application.
2. A copy of the report and its annexes, if any, is being transmitted to the International Bureau for communication to all the elected Offices.
3. Where required by any of the elected Offices, the International Bureau will prepare an English translation of the report (but not of any annexes) and will transmit such translation to those Offices.

4. REMINDER

The applicant must enter the national phase before each elected Office by performing certain acts (filing translations and paying national fees) within 30 months from the priority date (or later in some Offices) (Article 39(1)) (see also the reminder sent by the International Bureau with Form PCT/IB/301).

Where a translation of the international application must be furnished to an elected Office, that translation must contain a translation of any annexes to the international preliminary examination report. It is the applicant's responsibility to prepare and furnish such translation directly to each elected Office concerned.

For further details on the applicable time limits and requirements of the elected Offices, see Volume II of the PCT Applicant's Guide.

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PATENT COOPERATION TREATY

PCT

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Article 36 and Rule 70)

Applicant's or agent's file reference 4750/Deb 3	FOR FURTHER ACTION See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/416)	
International application No. PCT/GB00/00871	International filing date (day/month/year) 09/03/2000	Priority date (day/month/year) 10/03/1999
International Patent Classification (IPC) or national classification and IPC C09D5/03		
Applicant INTERNATIONAL COATINGS LIMITED et al.		
<p>1. This international preliminary examination report has been prepared by this International Preliminary Examining Authority and is transmitted to the applicant according to Article 36.</p> <p>2. This REPORT consists of a total of 5 sheets, including this cover sheet.</p> <p><input checked="" type="checkbox"/> This report is also accompanied by ANNEXES, i.e. sheets of the description, claims and/or drawings which have been amended and are the basis for this report and/or sheets containing rectifications made before this Authority (see Rule 70.16 and Section 607 of the Administrative Instructions under the PCT).</p> <p>These annexes consist of a total of 2 sheets.</p>		
<p>3. This report contains indications relating to the following items:</p> <p>I <input checked="" type="checkbox"/> Basis of the report</p> <p>II <input type="checkbox"/> Priority</p> <p>III <input type="checkbox"/> Non-establishment of opinion with regard to novelty, inventive step and industrial applicability</p> <p>IV <input type="checkbox"/> Lack of unity of invention</p> <p>V <input checked="" type="checkbox"/> Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement</p> <p>VI <input type="checkbox"/> Certain documents cited</p> <p>VII <input checked="" type="checkbox"/> Certain defects in the international application</p> <p>VIII <input checked="" type="checkbox"/> Certain observations on the international application</p>		
Date of submission of the demand 29/09/2000	Date of completion of this report 12.06.2001	
Name and mailing address of the international preliminary examining authority:  European Patent Office D-80298 Munich Tel. +49 89 2399 - 0 Tx: 523656 epmu d Fax: +49 89 2399 - 4465	Authorized officer Lux, R Telephone No. +49 89 2399 8593 	

**INTERNATIONAL PRELIMINARY
EXAMINATION REPORT**

International application No. PCT/GB00/00871

I. Basis of the report

1. With regard to the **elements** of the international application (*Replacement sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this report as "originally filed" and are not annexed to this report since they do not contain amendments (Rules 70.16 and 70.17)*):

Description, pages:

1-33 as originally filed

Claims, pages:

34-37,40-46 as originally filed

38,39 as received on 21/03/2001 with letter of 20/03/2001

2. With regard to the **language**, all the elements marked above were available or furnished to this Authority in the language in which the international application was filed, unless otherwise indicated under this item.

These elements were available or furnished to this Authority in the following language: , which is:

- ☐ the language of a translation furnished for the purposes of the international search (under Rule 23.1(b)).
☐ the language of publication of the international application (under Rule 48.3(b)).
☐ the language of a translation furnished for the purposes of international preliminary examination (under Rule 55.2 and/or 55.3).

3. With regard to any **nucleotide and/or amino acid sequence** disclosed in the international application, the international preliminary examination was carried out on the basis of the sequence listing:

- ☐ contained in the international application in written form.
☐ filed together with the international application in computer readable form.
☐ furnished subsequently to this Authority in written form.
☐ furnished subsequently to this Authority in computer readable form.
☐ The statement that the subsequently furnished written sequence listing does not go beyond the disclosure in the international application as filed has been furnished.
☐ The statement that the information recorded in computer readable form is identical to the written sequence listing has been furnished.

4. The amendments have resulted in the cancellation of:

- ☐ the description, pages:
☐ the claims, Nos.:
☐ the drawings, sheets:

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No. PCT/GB00/00871

5. ☐ This report has been established as if (some of) the amendments had not been made, since they have been considered to go beyond the disclosure as filed (Rule 70.2(c)):

(Any replacement sheet containing such amendments must be referred to under item 1 and annexed to this report.)

6. Additional observations, if necessary:

V. Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

1. Statement

Novelty (N)	Yes:	Claims	1-68
	No:	Claims	
Inventive step (IS)	Yes:	Claims	1-68
	No:	Claims	
Industrial applicability (IA)	Yes:	Claims	1-68
	No:	Claims	

2. Citations and explanations
see separate sheet

VII. Certain defects in the international application

The following defects in the form or contents of the international application have been noted:
see separate sheet

VIII. Certain observations on the international application

The following observations on the clarity of the claims, description, and drawings or on the question whether the claims are fully supported by the description, are made:
see separate sheet

1 2 3 4 5

6

**INTERNATIONAL PRELIMINARY
EXAMINATION REPORT - SEPARATE SHEET**

International application No. PCT/GB00/00871

Re Item V

Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

Powder coating compositions having the specific particle size features as defined in (1) and (2) of the independent claims of this application, and wherein the individual particulate materials are fused or bonded into composite particles, are not suggested in the art.

A wide range of reduced-gloss finishes avoiding the problems of conventional compositions (cf. page 2 of this application) is accessible with these new compositions.

This gloss-reduction can be achieved with substantially different proportions of gloss-reducing additives. The agglomerated material does not suffer from particle segregation in the solid state as would dry-blended products, thus giving uniformity of product even after transportation and application (spraying).

Further, maximising the level of larger-sized uncoloured components, which are surprisingly not discernable by the unaided human eye, gives cost advantages.

Therefore, the requirements of Art. 33 (2)/(3) PCT are met.

Re Item VII

Certain defects in the international application

Expression not being in line with the scope of the claims such as "for example" (cf. page 7 line 4) etc. could lead to misinterpretation and thus should not be present in the description.

**INTERNATIONAL PRELIMINARY
EXAMINATION REPORT - SEPARATE SHEET**

.International application No. PCT/GB00/00871

Re Item VIII

Certain observations on the international application

The claims are deficient having regard to the requirements of Art. 6 PCT.

All independent claims are silent as to the size of the "agglomerates" of the individual particulate components fused or bonded together into composite particles. Apparently, the particles are air-fluidisable and can be applied to a substrate by electrostatic spray (cf. page 7 lines 23-25). This feature seems to be essential to this invention?

Claim 55 is unclear due to the term "higher" used in conjunction with the Dv.50 value (see line 8 of page 44). Obviously, "higher" refers to the corresponding Dv value of the differently coloured film-forming base components?

The Dv. value of the differently coloured film-forming base components is not specified in claim 59 and thus an essential feature (see remaining independent claims) is missing.

Claims 64/65 are unclear due to the vague term "agglomerating" (which means? fusing or bonding etc.?).

Claim 67 is unclear due to the vague term "continuous". This relative term is open to speculations (variation in thickness and/or roughness? etc.).

- 38 -

16. A powder coating composition as claimed in claim 15, wherein the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2a) is in the range of from 1:99 to 40:60 by weight.

5 17. A powder coating composition as claimed in claim 16, wherein the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2a) is in the range of from 1:99 to 30:70 by weight.

10 18. A powder coating composition as claimed in claim 17, wherein the ratio of coloured film-forming base components (1) to uncoloured film-forming component(s) (2a) is in the range of from 5:95 to 30:70.

15 19. A powder coating composition as claimed in any one of claims 1 to 18, wherein the uncoloured film-forming component or components (2) are present in an amount of at least 50% by weight of the total film-forming components.

20 20. A powder coating composition as claimed in claim 19, wherein the uncoloured film-forming component or components (2) are present in an amount of at least 60% by weight of the total film-forming components.

21. A powder coating composition as claimed in claim 20, wherein the uncoloured film-forming component or components (2) are present in an amount of at least 70% by weight of the total film-forming components.

25 22. A powder coating composition as claimed in any one of claims 2 to 21, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 20% by weight of the total film-forming components.



- 39 -

23. A powder coating composition as claimed in claim 22, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 30% by weight of the total film-forming components.

5

24. A powder coating composition as claimed in claim 23, wherein the uncoloured film-forming component or components (2a) are present in an amount of at least 40% by weight of the total film-forming components.

10

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15

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20

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25

28. A powder coating composition as claimed in any one of claims 1 to 27, wherein there are two or more compatible coloured film-forming base components (1).

29. A powder coating composition as claimed in any one of claims 1 to 28, wherein the uncoloured film-forming component (2a) or at least one of the uncoloured

PATENT COOPERATION TREATY

PCT

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Article 36 and Rule 70)





Applicant's or agent's file reference 4750/Deb 3	FOR FURTHER ACTION See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/416)	
International application No. PCT/GB00/00871	International filing date (day/month/year) 09/03/2000	Priority date (day/month/year) 10/03/1999
International Patent Classification (IPC) or national classification and IPC C09D5/03		
Applicant INTERNATIONAL COATINGS LIMITED et al.		

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- I ☒ Basis of the report
- II ☐ Priority
- III ☐ Non-establishment of opinion with regard to novelty, inventive step and industrial applicability
- IV ☐ Lack of unity of invention
- V ☒ Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
- VI ☐ Certain documents cited
- VII ☒ Certain defects in the international application
- VIII ☒ Certain observations on the international application

Date of submission of the demand 29/09/2000	Date of completion of this report 12.06.2001
Name and mailing address of the international preliminary examining authority:  European Patent Office D-80298 Munich Tel. +49 89 2399 - 0 Tx: 523656 epmu d Fax: +49 89 2399 - 4465	Authorized officer Lux, R Telephone No. +49 89 2399 8593 

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No. PCT/GB00/00871

I. Basis of the report

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Claims, pages:

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INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No. PCT/GB00/00871

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	No:	Claims	
Inventive step (IS)	Yes:	Claims	1-68
	No:	Claims	
Industrial applicability (IA)	Yes:	Claims	1-68
	No:	Claims	

2. Citations and explanations
see separate sheet

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see separate sheet

VIII. Certain observations on the international application

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see separate sheet

Re Item V

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A wide range of reduced-gloss finishes avoiding the problems of conventional compositions (cf. page 2 of this application) is accessible with these new compositions. This gloss-reduction can be achieved with substantially different proportions of gloss-reducing additives. The agglomerated material does not suffer from particle segregation in the solid state as would dry-blended products, thus giving uniformity of product even after transportation and application (spraying).

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Re Item VII

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**INTERNATIONAL PRELIMINARY
EXAMINATION REPORT - SEPARATE SHEET**

International application No. PCT/GB00/00871

Reason VIII

Certain observations on the international application

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The Dv. value of the differently coloured film-forming base components is not specified in claim 59 and thus an essential feature (see remaining independent claims) is missing.

Claims 64/65 are unclear due to the vague term "agglomerating" (which means? fusing or bonding etc.?).

Claim 67 is unclear due to the vague term "continuous". This relative term is open to speculations (variation in thickness and/or roughness? etc.).

INTERNATIONAL SEARCH REPORT

International Application No
PCT/GB 00/00871

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 C09D5/03

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 C09D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WO 91 18951 A (COURTAULDS COATINGS) 12 December 1991 (1991-12-12) page 40, line 23 -page 43, line 5 page 52, line 20-24 page 53, line 19 -page 54, line 1 & EP 0 539 385 A cited in the application ---	1-68
A	EP 0 459 048 A (COURTAULDS COATINGS) 4 December 1991 (1991-12-04) page 3, line 20-39 ---	1, 6, 55, 59, 64-68
A	PATENT ABSTRACTS OF JAPAN vol. 012, no. 159 (C-495), 14 May 1988 (1988-05-14) & JP 62 270672 A (ASAHI CHEM IND CO LTD), 25 November 1987 (1987-11-25) abstract -----	

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

* Special categories of cited documents :

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

- "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- "&" document member of the same patent family

Date of the actual completion of the international search

8 June 2000

Date of mailing of the international search report

21/06/2000

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
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Fax: (+31-70) 340-3016

Authorized officer

Girard, Y

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/GB 00/00871

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
WO 9118951 A	12-12-1991	AT 129275 T	15-11-1995
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TENT COOPERATION TREATY

PCT

INTERNATIONAL SEARCH REPORT

(PCT Article 18 and Rules 43 and 44)

Applicant's or agent's file reference 4750/Deb 3	FOR FURTHER ACTION see Notification of Transmittal of International Search Report (Form PCT/ISA/220) as well as, where applicable, item 5 below.	
International application No. PCT/GB 00/ 00871	International filing date (day/month/year) 09/03/2000	(Earliest) Priority Date (day/month/year) 10/03/1999
Applicant INTERNATIONAL COATINGS LIMITED et al.		

This International Search Report has been prepared by this International Searching Authority and is transmitted to the applicant according to Article 18. A copy is being transmitted to the International Bureau.

This International Search Report consists of a total of 2 sheets.

☒ It is also accompanied by a copy of each prior art document cited in this report.

1. Basis of the report

- a. With regard to the **language**, the international search was carried out on the basis of the international application in the language in which it was filed, unless otherwise indicated under this item.

☐ the international search was carried out on the basis of a translation of the international application furnished to this Authority (Rule 23.1(b)).

- b. With regard to any **nucleotide and/or amino acid sequence** disclosed in the international application, the international search was carried out on the basis of the sequence listing:

☐ contained in the international application in written form.

☐ filed together with the international application in computer readable form.

☐ furnished subsequently to this Authority in written form.

☐ furnished subsequently to this Authority in computer readable form.

☐ the statement that the subsequently furnished written sequence listing does not go beyond the disclosure in the international application as filed has been furnished.

☐ the statement that the information recorded in computer readable form is identical to the written sequence listing has been furnished

2. ☐ **Certain claims were found unsearchable** (See Box I).

3. ☐ **Unity of invention is lacking** (see Box II).

4. With regard to the **title**,

☒ the text is approved as submitted by the applicant.

☐ the text has been established by this Authority to read as follows:

5. With regard to the **abstract**,

☒ the text is approved as submitted by the applicant.

☐ the text has been established, according to Rule 38.2(b), by this Authority as it appears in Box III. The applicant may, within one month from the date of mailing of this international search report, submit comments to this Authority.

6. The figure of the **drawings** to be published with the abstract is Figure No.

☐ as suggested by the applicant.

☐ because the applicant failed to suggest a figure.

☐ because this figure better characterizes the invention.

☒ None of the figures.

INTERNATIONAL SEARCH REPORT

International Application No
PCT/GB 00/00871

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 C09D5/03

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 C09D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	W0 91 18951 A (COURTAULDS COATINGS) 12 December 1991 (1991-12-12) page 40, line 23 -page 43, line 5 page 52, line 20-24 page 53, line 19 -page 54, line 1 & EP 0 539 385 A cited in the application ----	1-68
A	EP 0 459 048 A (COURTAULDS COATINGS) 4 December 1991 (1991-12-04) page 3, line 20-39 ----	1,6,55, 59,64-68
A	PATENT ABSTRACTS OF JAPAN vol. 012, no. 159 (C-495), 14 May 1988 (1988-05-14) & JP 62 270672 A (ASAHI CHEM IND CO LTD), 25 November 1987 (1987-11-25) abstract -----	

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

° Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

Date of the actual completion of the international search

8 June 2000

Date of mailing of the international search report

21/06/2000

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INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/GB 00/00871

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
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			JP 3015946 B	04-03-1991

